

Experimental Design of a 1.5KVA UPS Unit Using Locally Obtainable Materials under Prevailing Academic Laboratory Condition in Nigeria

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Abstract—This study is aimed at designing, fabrication and evaluation of an efficient UPS based on locally obtainable material and conditions, for local application in academic environments. From a load survey, a load of 1.2 kW was obtained for Nigeria academics offices, which lead to the design of a 1.5 kVA UPS. A standard oscillating circuit based on CD4047 was adopted and adapted in the design. By loading requirements, 8 units of IRF250 MOSFETs were evaluated for the design. To improve the reliability (increase time to failure of battery) and effectiveness of the design, a battery charging controller and level detector were evaluated for addition to the design. The oscillatory circuit was tested using oscilloscope, and the open circuit and short circuit tests of the designed transformer for the construction was carried to define its efficiency. From the design, a square waveform of output voltage was obtained. The designed transformer efficiency obtained for the designed UPS is approximately 82%. A comparative technical and costs assessment show that the constructed UPS is cheaper but of less efficiency when compared with the imported 1.5 kVA products available in the Nigerian market.

Keywords—UPS, Efficiency, Cost, Local Design, Office Load, Nigeria.

I. INTRODUCTION

There are economic, social, technical and environmental challenges in trying to satisfy the demand of electricity by consumers in a developing economy. Alternating current power problems have been recognized by the utility companies, computer manufacturers and end users as a subject that must be addressed. The power problems extend from spikes, noise and frequency variations to complete black-outs. These problems can be corrected individually using surge suppressors, filters, regulators, and amplifiers, but only Uninterruptible Power System (UPS) can solve all these problems collectively [1]. The UPS is a unit composing of a range of solid-state devices, are interconnected based on their respective functional principles to provide required unit function of protection against supply aberrations and failure for the critical. Because these units are composed of solid-state devices they are often described as static UPS units, as opposed to rotary systems which are based on motor/generator technology[2].

An UPS typically does two things[3]: It either provides power to enable the safe shutdown of equipment and saving data to a non-volatile

medium, or it provides power to equipment over the duration of mains fault/failure, enabling equipment to operate continuously. Continuous operation is primarily a function of load drawn and battery type and size. Basically, an UPS unit converts some or all of the AC power from the mains into DC for storage in a battery and then back into AC power for the load when there is mains failure. This double conversion has many variations; however, all of the existing designs incorporate an inverter to convert DC into AC. It is the inverter operation which defines an UPS as on-line (operates only when needed) or off-line (operates continuously) [3].

The study is motivated by the unbearable discomfort to productivity and cost of power interruption in Nigeria academic environment where the availability of power supply is needed at all times. The local market is fully of numerous imported UPS devices with no local content or brands. Experimental studies for local brands are therefore crucial economically to Nigerian power supply conditions and reduction in dependence on imported brands.

The aim of this study is to obtain a locally made UPS system that can cover a 1.5 kVA academic office load that can efficiently substitute imported brands of the same rating within Nigeria. The specific aims are to design and construct the UPS system under prevailing local laboratory conditions for comparative analysis with available imported brands in terms of cost and energy efficiency only.

II. OPERATION PRINCIPLE OF AN UNINTERRUPTIBLE POWER SUPPLY SYSTEM

The principle of operation uninterruptible power supply system depends on whether the UPS is off-line or on-line. It is off-line when the UPS operates only when needed and then it is on-line, when it operates continuously [4]. The one adopted in the design was the off-line or stand-by mode. The Stand by UPS technology is shown in Fig. 1. The utility power in the off-line mode feeds the load and the disconnect switch (solid state or electro-mechanical) is connected directly to the load. The Charger is on, keeping the battery under charge. During this stage, the Inverter is off and no voltage or frequency regulation for 4 to 10 millisecond transfer time (with break on the output). This is simple and reliable, cost-effective performance

and suitable for protecting workstations. The major drawbacks are: impractical above 2.2 kVA, unsuitable for industrial or extreme environments or where poor voltage regulation is present, and heavy above 500 VA. The block diagram for the UPS components is shown in Fig. 2.

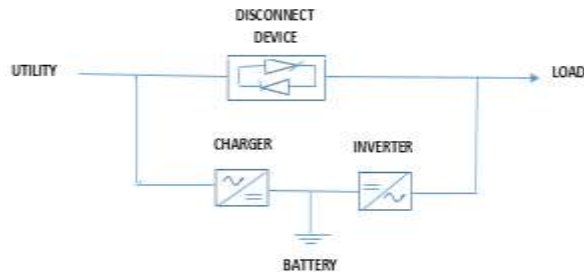


Fig. 1 The Standby/ off-line UPS

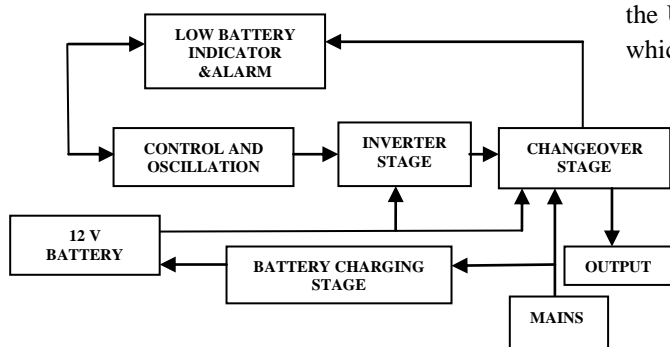


Fig. 2 The block diagram of the UPS System

From Figure 1, when the UPS system is on off-line mode of operation, the above block diagram above indicates the flows of operation. The utility main supplies the battery charger stage as well as the load from the output end when the main is on. And when the main is off, the battery supply 12V to the inverting stage which is responsible for the conversion of D.C voltage to A.C voltage. It consists of power switching devices which are as follows: MOSFET, resistors, diodes. This is driven by control circuitry of the control stage. The output from each half circuit of the inverter is connected to a center-tap transformer that commutates the output voltage and steps it up to the required mains voltage. The oscillatory stage is responsible for control of the switching's devices in the inverter stage. It generate out of phase pulse trains to drive the MOSFET switches in the inverter stage. It also determines the frequency of operation i.e. the frequency of the output waveform from the inverter transformer. To ensure the automation of the change in supply from either the main to the battery or vice versa, the changeover stage which is comprises of relays is used with several sets of contact to perform the changeover function. The relay is enabled (energized) by the presence of mains voltage. The Low battery indicator circuit and alarm circuit provide visual indication of low battery level. An LED serves as the indicating devices. It comes 'ON' at a predetermined battery voltage level before the UPS

shut down (if continued to be used), while the alarm circuit serves as an sound indicator when power supply is 'ON' and 'OFF' and also when the battery start its backup [4].

III.METHODOLOGY

As earlier discussed, a UPS design is made-up of different stages. The design process of each stage is discussed in this section.

A. Selection of the UPS Rating

From a load survey of academic offices in a Nigerian Federal University, typical electric appliances (EAs) and quantities (Qty) were obtained for UPS unit sizing as shown in Table 1. The rating of the UPS was based on the chosen area of application, which is an office in an academic environment.

Table I

Total Load Specification for the Office

EAs	Unit Load(W)	Qty of EA	Total Load(W)
EA	P_U	N_U	P_{EA}
Television Set	100	1	100
Computer/Laptop	200	2	400
Printer	200	1	200
Fan	80	2	160
Florescent Tube	60	4	240
Miscellaneous	100	1	100
Total	740	11	1200

The UPS capacity rating can be obtained from the equation .1 [5]:

$$\text{Active Power(W)} = \text{Apparent Rating(VA)} \times \text{Powerfactor} \quad 1$$

Using a power factor of 0.8[6],

$$\text{Apparent Rating} = 1500\text{VA} = 1.5\text{kVA}$$

The miscellaneous rating in the table above caters for additional rating that may be needed.

B. Oscillation stage

For the oscillation stage, 4047 integrated circuit(IC) was used. It generates a square wave and this determines the frequency of the pulse at the output of the oscillator. This will only be achieved when connected with some external components such as capacitors, resistors, 7812 and 7815 regulators and transistors [7] as shown in fig. 3.

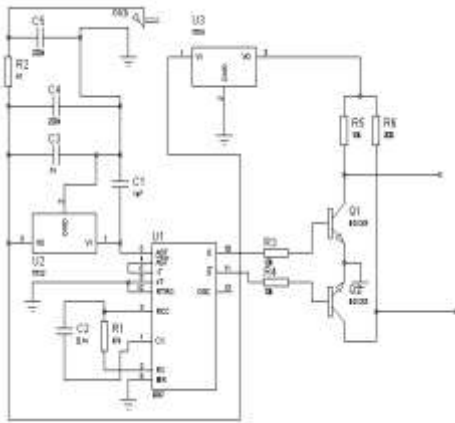


Fig.3 CD4047 Circuit Layout

From CD4047 data sheet [7], the maximum capacitance that can be used in the layout is 50pF at 200kΩ, therefore a capacitor (C₂) of value 0.1μF was used. A frequency of 50Hz was chosen as the pulse frequency owing to the fact that the expected sine wave frequency will be 50Hz. The relationship between the capacitor and the resistor is given by the equation 2 [7].

$$T = \frac{4.40R_1C_2}{2}$$

where, T is the period and hence, the resistor value (R₁) can now be calculated to be 50kΩ.

C. Inverter/Driver stage

The driver used for this project is MOSFET based due to the fact that it does not suffer from thermal breakdown and majorly it aids paralleling since it has a positive on-resistance unlike bipolar transistor which will require a current equalising resistor [8]. MOSFET (IRF250) was used for the design, paired in parallel as shown in figure 4 to ensure a maximum power transfer. Equation 3 [9] was used to calculate the number of MOSFET required.

$$N_o = \frac{\text{UPS handling capacity}}{\text{MOSFET maximum power dissipation}}$$

where IRF250 maximum power dissipation is 150W, N_o = 8.

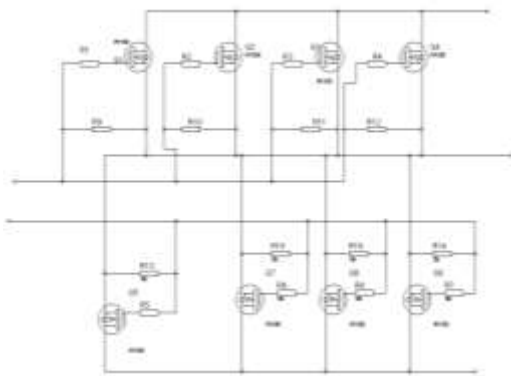


Fig. 4 MOSFET Paralleling Circuit.

Each of the MOSFET was mounted on a heat sink in order to keep the temperature of the semi-conductor below 125°C [10]. To calculate the required thermal resistance of the heat sink, equation 4[10] was used.

$$R_{th} = \frac{T_j - T_c}{P_D}$$

where, T_j is the junction temperature and T_c is the case temperature.

$$T_j = 125^\circ\text{C}, T_c = 25^\circ\text{C} [10]$$

D. Battery charging stage and battery level detector

The circuit layout of the battery charging is shown in figure 5. Transformer T₁ steps down the mains voltage from 240V to 12V. The 12V A.C voltage from the transformer is passed through a power bridge rectifier D1-D4 to provide full rectification. Power resistor R₁ helps to limit the charging current to a safe value and diodes D6 prevents the battery from discharging back into the bridge rectifier and the transformer during mains failure. This also helps to avoid the LED becoming lit.

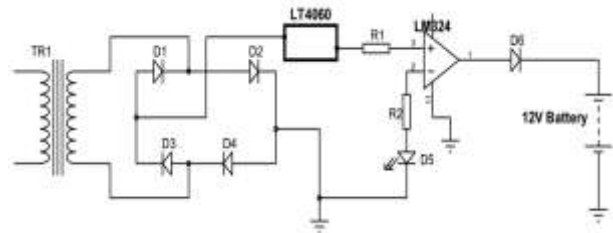


Fig.5 Battery Charging Circuit

LTC 4060 which serve as the charger control automatically senses the DC input supply and battery insertion or removal. Heavily discharged batteries are initially charged at C/5 (battery capacity per 5 hours) rate before a fast charge is applied. Fast charge is terminated using the -ΔV detection method [11]. Backup termination consists of a programmable timer and battery overvoltage detector.

The battery level detector employs the use of LM324 output comparator IC which compares the battery voltage with a reference voltage at different levels and produces their corresponding output which energizes the Light emitting diode (LED) to show the battery level. It consists of four operation amplifiers which acts as a follower circuit with all the inverting pins gated with 1k and then grounded. In this design, the four voltage levels are indicated by four light LED in a vertical array listed in Table 2.

Table II
Led Indicators

VOLTAGE LEVEL	LED INDICATOR
HIGH	RED
MEDIUM	GREEN
LOW	YELLOW
SHUT DOWN	WHITE

E. Changeover stage

The changeover stage was designed for automatic control of its mechanism with the aid of a relay. The relay used for this design is FANGKE JZC- 23F (4123) with specification given as 10A/28Vdc, 2.8 Ω, dc 12V. In this design, five relays of 12 V were used.

F. Transform Design

1) Design Requirement

The transformer requirements used to step up the battery voltage from 12V to 220V were calculated based on the UPS rating. These are then summarised in the Table 3.

Table III
The Transformer Requirements

Transformer Requirement	Calculated Value
Primary Voltage	12V
Secondary Voltage	220V
Primary current	125A
Secondary current	682A
Primary winding wire gauge	SWG12
Secondary winding wire gauge	SWG22
Number of secondary turns	504 turns
Number of Primary turns	28turns

2) Transformer efficiency

The total loss in a transformer is given as 5 [5]

$$\Delta P_T = \Delta P_{FE} + \Delta P_{CU}$$
 5

where ΔP_{FE} is the iron loss, and ΔP_{CU} is the copper loss. The values of ΔP_{FE} and ΔP_{CU} were obtained from open circuit and short circuit tests respectively.

The Efficiency (ζ) of transformer is obtained as,

$$\zeta = \left(1 - \frac{\Delta P_T}{P_{in}}\right) \times 100\%$$
 6

where P_{in} is the input power to the UPS.

$$P_{in} = V_{in} \times I_{in}$$
 7

where V_{in} and I_{in} are the input voltage and current to the UPS respectively. The obtained values of ΔP_{FE} , ΔP_{CU} , ΔP_T , V_{in} , I_{in} , P_{in} and ζ are presented in Table 4.

G. Comparative efficiency and cost analysis

The constructed UPS was compared with existing UPS of the same rating in Nigeria market. The comparison was carried out in terms of efficiencies and costs of the UPS.

1) Comparison in term of efficiencies

The range of the market efficiency (ζ_m) for a 1.5kVA rated UPS according to [12] is from 95% to 99%. The efficiency of the constructed UPS as shown in table 4 is 82%. The efficiency comparison factor (α) is given as,

$$\alpha = \frac{\Delta \zeta_m^{min}}{\zeta_m^{min}} \text{ to } \frac{\Delta \zeta_m^{max}}{\zeta_m^{max}} = \frac{\zeta_m^{min} - \zeta_c}{\zeta_m^{min}} \text{ to } \frac{\zeta_m^{max} - \zeta_c}{\zeta_m^{max}}$$
 8

where, ζ_m^{max} is the market maximum efficiency, ζ_c is the efficiency of the constructed UPS, ζ_m^{min} is the market minimum efficiency, $\Delta \zeta_m^{min}$ and $\Delta \zeta_m^{max}$ is the minimum and maximum difference in efficiencies between imported and constructed UPS. The obtained values of ζ_m^{max} , ζ_m^{min} , ζ_c , $\Delta \zeta_m^{min}$, $\Delta \zeta_m^{max}$ and α is shown in Table 5.

2) Comparison in term of cost

The range of the Market Cost of Imported C_m for a 1.5kVA rated UPS according to [12] is from ₦12,000 - ₦15,000. The cost of the constructed UPS is ₦10,000. The cost comparison factor (β) is given as,

$$\beta = \frac{\Delta C_m^{min}}{C_m^{min}} \text{ to } \frac{\Delta C_m^{max}}{C_m^{max}} = \frac{C_m^{min} - C_c}{C_m^{min}} \text{ to } \frac{C_m^{max} - C_c}{C_m^{max}}$$
 9

where, C_m^{max} is the market maximum cost, C_c is the cost of the constructed UPS, C_m^{min} is the market minimum cost, ΔC_m^{min} and ΔC_m^{max} is the minimum and maximum difference in cost between imported and constructed UPS. The obtained values of C_m^{max} , C_m^{min} , C_c , ΔC_m^{min} , ΔC_m^{max} and β is shown in Table 6.

IV. RESULT AND DISCUSSION

A. Experimental Results and Discussion

Test was carried out on each stage of the inverter. The oscillator stage and the inverting stage were tested using an oscilloscope and their results are shown in fig. 6.

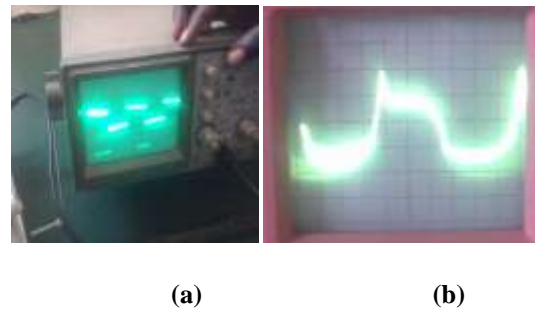


Fig. 6 Results from the oscilloscope

The output from an oscillator, shown in fig. 6a is a square wave which is produced by the astable mode in the oscillator. This is needed in order to get the equivalent sine wave shown in fig. 6b. The conversion of the sine wave was carried out by the inverting stage of the system which consists of four pair of MOSFET.

Table 4 presents the result obtained the short circuit test and open circuit test carried out on the constructed transformer. The result shows an efficiency of 82%, obtained from calculation.

Table IV
Transformer Test and Efficiency Result

ΔP_{FE} (W)	ΔP_{CU} (W)	ΔP_T (W)	V_{in} (V)	I_{in} (A)	P_{in} (W)	ζ %
20.8	200	220.8	220	5.45	1200	82

Fig. 7 shows the relationship between the copper loss and the input voltage obtained when the short circuit test setup input voltage was varied. From the graph, it was observed that the minimum loss is at 20V. This then suggests that the input voltage must be above 20V.

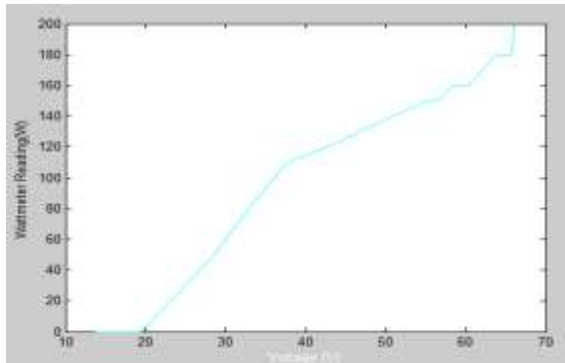


Fig. 7 The Relationship between the Copper Loss and the Input Voltage

Table V
Result of comparison in terms of efficiency

ζ_m^{min} (%)	ζ_m^{max} (%)	ζ_c (%)	$\Delta\zeta^{min}$ (%)	$\Delta\zeta^{max}$ (%)	α
95	99	82	13	17	0.14 to 0.17

Table VI
Result of comparison in terms of cost

C_m^{min} (₦)	C_m^{max} (₦)	C_c (₦)	ΔC^{min} (₦)	ΔC^{max} (₦)	β
12,000	15,000	10,000	2,000	5,000	0.167 to 0.333

From Table 5, the value of α obtained implies that the efficiency of imported UPS in Nigeria market is greater than the constructed one by approximately 14 to 17%. Also from table 6, the value of β obtained indicates that the imported UPS are costlier than the locally constructed UPS by approximately 17 to 33%.

V. CONCLUSION

The Uninterruptible Power Supply of 1.5kVA, 1.2kW, 12V was designed for application as a backup power source for a typical load in an academic office using locally available materials and under academic laboratory condition. The design procedure in each stage of the UPS was well presented in detail. The efficiency of the designed transformer was obtained to

be 82%, and from a comparative analysis in terms of cost and efficiencies between imported UPS in Nigeria market and the constructed UPS using the proposed metrics of α and β , it was observed that the imported UPS is of higher efficiency than the constructed UPS by 14 to 17%, but also costlier than the constructed UPS by 17 to 33%. From the comparison results, it can be implied that the differences in the efficiencies can be compensated for if the laboratory condition of the constructed UPS is improved upon to be of the same or better condition as that of the imported UPS.

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