

# Hysteresis Controller Based Enhanced Photo Voltaic System for Ac Applications

Ch Bhanu Pratap<sup>1</sup>, M Phani Raju<sup>2</sup>

*1*pursuing M.Tech (EEE), *2*working as Assistant Professor (EEE),  
Nalanda Institute Of Engineering and Technology (NIET)Kantepudi(V), Sattenpalli(M), Guntur (D)-  
522438,Andhra Pradesh.

## Abstract

The fly back converter has the huge merits like as compressed conformation, trouble-free control loop, electric separation, high step-up ratio, high reliability and performance, etc. So it is a permissive and effective technology for compensating problems for the Ac Applications. In this paper boundary conduction mode (BCM) of operation utilizing rather than the CCM and DCM. Because of it's operated under wide range of frequencies. Then it will produce less ripple contents in the output, it will maintained high efficiency levels. Nevertheless, the BCM controller is very difficult because they have different switching mode operating frequency conditions. This may happens to complications in the models it will leads to difficulties in the mathematical simplifications between output current  $i_{out}$  and the reference required current  $i_{ref}$ , which has a huge manipulation on the THD of  $i_{out}$ . This paper involves and implemented a calculation model between output current  $i_{out}$  and  $i_{ref}$  reference current in BCM during theoretical beginning knowledge, and developed a simplified control strategy to make the reference current shows that has to be maintaining decreases THD of output current. Temporarily the understanding of Hysteresis controller based on the analyzed model is also founded. As results the simulation models are tested and verified within the MATLAB/SIMULINK are demonstrated, which delivers the implemented approach has the effective model for ac applications.

**Keywords** — AC module, energy conversion, photovoltaic power systems, system analysis and design, hysteresis controller.

## I. INTRODUCTION

Photovoltaic air conditioning module (PV ACM), likewise named as smaller scale inverter [1], is a minimal and measured structure for small power PV era framework applications [2]. This concept was conceived 30 years back at Caltech's Jet Propulsion Laboratory [3]. Be that as it may, it is just as of late coming to commercial realization.

These days, it's perceived as an appealing solution for the private utility-intuitive PV frameworks [4]. PV ACM is characterized as the combination of a solitary PV panel and a solitary stage framework tied (GT) inverter [5]. The GT

inverter is the immediate interface between the PV board and the residential utility, which changes over the low dc voltage from the PV board to the higher air conditioning voltage of the lattice.

Contrasted with the conventional single-or multi string inverters in PV applications, advantages of PV ACM incorporate more adaptability and less establishment cost in framework development as an "attachment and play" gadget, lower manufacturing cost through large scale manufacturing, absence of the force mismatch between PV modules, and higher framework level energy harvesting capacity under shaded conditions [6].

In any case, the PV ACM must meet a progression of brutal requirements, such as THD and islanding assurance requested by standards of GT gadgets, most extreme force point track (MPPT) and least power variance requested by PV boards, high efficiency, high dependability, long lifetime, ease, and simple establishment requested by clients [7].

For fulfilling these unforgiving necessities, numerous topologies and control strategies have been accounted for in references [8]. Nowadays, a solitary stage flies back-sort utility intuitive inverter, which consolidated a voltage-controlled current-source fly back and a GT inverter as one single stage [9], is regarded as an appealing arrangement in PV ACM applications. Its major advantages incorporate electric confinement, high power thickness, high efficiency, and high stride up proportion, which depend on the simple control circle and smaller structure [10].

In any case, its large input limit and loss of spillage inductance vitality are still the challenges for architects. At present, more works have been done on the change for the fly back inverter, for example, control circle, force decoupling, delicate exchanging, and MPPT control.

In three operation modes [11] (CCM, DCM, and BCM) of the fly back inverter are examined in the PV ACM applications. CCM can be acknowledged with normal current control. However, the crest current control of the auxiliary current is not proper for CCM, since the transformer is incompletely demagnetized amid every exchanging cycle, and the

framework will behave as a heap autonomous voltage source with top current control [12].

Additionally, the fly back inverter at light load will slip into DCM operation around the zero intersection of network voltage, which builds the trouble of control framework outline.

DCM and BCM can be effortlessly acknowledged with top current control [13], which has no stage postponement contrasted with the average current control. In the interim, DCM and BCM have the ZCS feature naturally, so can have higher productivity in correlation with CCM operation. Moreover, the force thickness of BCM is generally higher than DCM. Thus, BCM is more preferred for PV ACM applications considering all the prior research works.

In the BCM with crest current control, the yield current  $i_{out}$  is specifically controlled by the reference current  $i_{ref}$  amid each every exchanging cycle. Since the fly back inverter works as an ac current source, a variable exchanging recurrence (VSF) control procedure must be connected. In any case, the VSF fs lead to the difficulty to get the precise numerical model between  $i_{out}$  and  $i_{ref}$ . As the THD of  $i_{out}$  must agree to the norms of GT gadgets, the scientific model is critical in the outline of  $i_{ref}$ .

The motivation behind this paper is to examine and propose an accurate mathematical model in the middle of  $i_{out}$  and  $i_{ref}$  through theoretical derivation. In view of the proposed scientific model, the relationship in the middle of fs and  $i_{ref}$  is additionally broke down. At that point, a novel control technique of  $i_{ref}$  is proposed to decline THD of  $i_{out}$ . Besides, the acknowledgment of MPPT in light of this control strategy is likewise researched. At long last, the control procedure is verified based on an enhanced fly back-inverter topology [14]. Both recreation and investigation results on this topology are appeared in this paper.

This paper is composed as takes after. Theres identical utility-intuitive PV framework and the improved fly back-inverter topology utilized in this paper are depicted. The scientific model between  $i_{out}$  and  $i_{ref}$  in BCM by hypothetical derivation. The control technique of  $i_{ref}$  and fs for the improved fly back inverter in BCM operation. Area V examinations the realization of MPPT taking into account the proposed numerical model.

## II. IMPROVED FLYBACK-INVERTER TOPOLOGY

**A. Residential Utility-Interactive PV System:** The private PV framework has extraordinary

capability of being a significant market, because of taking after points of interest: [15] 1) interpreting the utility quality into a passable framework expense utilizing the property holder financial parameters and 2) the PV framework is capable to use the rooftop for bolster structure, dispensing with the area and direct structure costs. Fig. 1 shows the diagram of the residential utility-interactive PV framework in view of ACM gadget. In this framework, the PV exhibit is mounted on the client's rooftop, the purchaser's burden is joined at the air conditioner line terminal, and the ACM can be mounted on every individual PV board as a particular gadget. The accessible dc power from the PV board shifts with the sun powered light and encompassing temperature, is changed over to the

Single-stage 50/60 Hz air conditioning power and sustained to the utility line through ACM. In the daytime, the sunlight based force supplies to the shopper also, the surplus is sustained to the utility line, while in shady climate on the other hand after nightfall, and the utility line sustains the load.

### B. Fly Back Inverter:

Fig. 1 shows the topology of the fly back inverter, which comprises of three MOSFETs, two diodes, and a fly back transformer with focus tapped auxiliary winding. The two yields from the transformer are joined with the matrix, through a typical filter circuit, which can switch proportionally and synchronously with the extremity of the lattice voltage.

Henceforth, the fly back-inverter regulates the optional current into the collapsed sinusoidal current by  $S_{m1}$  en unravels it by  $S_{m2}$  furthermore,  $S_{m3}$ , and finally infuses the air conditioner current into the lattice through the output filter.

### C. Improved Fly Back-Inverter Topology

Fig. 2 shows the topology of the improved fly back inverter, which is described in. This topology involves an interleaved-fly back converter and a line-recurrence GT inverter. Its guideline is same as the essential fly back inverter. The interleaved-fly back converter regulates the auxiliary current into collapsed sinusoidal current. At that point, the current is developed and infused through the yield filter by the GT inverter. Actually, the enhanced topology is not as minimized as the essential fly back inverter, yet has taking after focal points:

- 1) The presented interleaved-fly back converter contains two fly backs, which can enhance the force rating drastically.
- 2) Every fly back is stage moved  $180^\circ$  in every exchanging cycle, as appeared in Fig. 4. This interleaved operation can accomplish comparable

twofold exchanging recurrence thus to decrease the auxiliary current swell.

3) The transformer with focus tapped optional winding is no required because of the free GT inverter, which can lessen the difficulty of transformer configuration. The voltage anxiety of optional switches is also decreased because of the GT inverter.

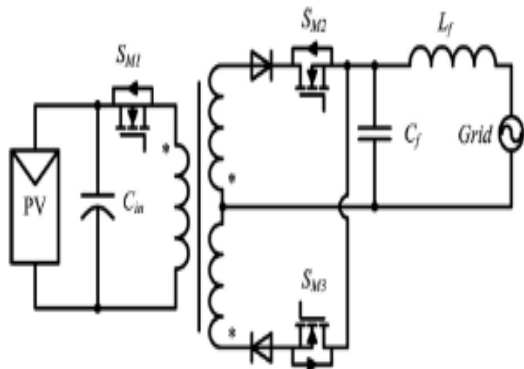


Fig. 1. Fundamental Fly Back-Inverter Topology.

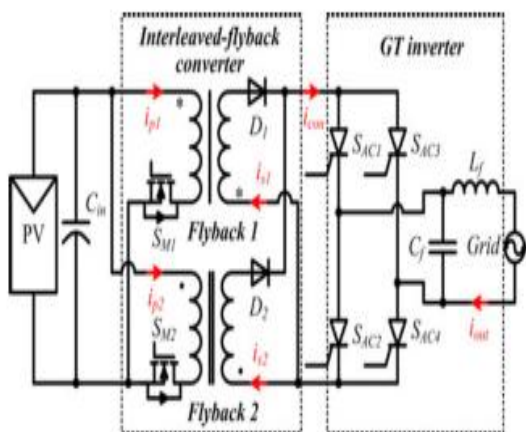


Fig. 2. Improved Fly Back Inverter Topology.

#### D. Mathematical Model of the BCM Operating fly back Inverter

This segment examines and proposes the scientific model between  $i_{out}$  out also,  $i_{ref}$  in a BCM working fly back inverter. Since the operation of the enhanced topology is the same as the basic topology, the accompanying investigation is for the most part based on the basic fly back inverter for simplification.

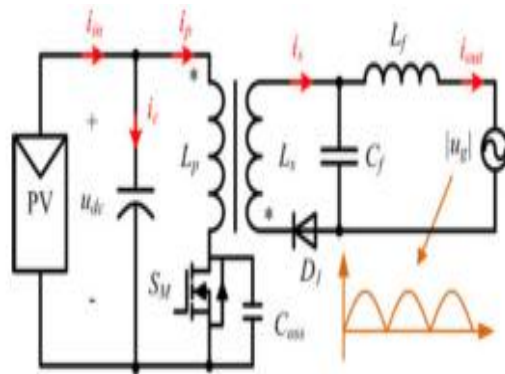


Fig. 3. Equivalent Diagram of a Single Fly Back Inverter.

#### E. BCM Operation

Because of the extremity exchanging circuit, the operations of the fly back inverter are the same amid both the positive and negative half cycle of the lattice voltage. In this way, the proportionate graph for a solitary fly back inverter can be appeared as Fig. 3. As indicated by this figure, the yield current  $i_{out}$  is acquired by filtering auxiliary current  $i_g$ .

In BCM operation, the crest esteem is  $i_p$  out of the essential current  $i_p$  is compelled to take after the reference current  $i_{ref}$ . Amid each exchanging cycle, when  $i_g$  declines to zero,  $S_m$  ref conducts, and this procedure can be acknowledged by semi full (QR) control. Whenever  $S_m$  switches on,  $i_p$  increments progressively in a direct connection with  $u_{dc}$ . When  $i_p$  equivalent to  $i_{ref}$ ,  $S_m$  is off and  $i$  diminishes directly with  $u_g$ . Along these lines, the relationship between  $i$  furthermore,  $i_{ref}$  in BCM amid half one cycle is appeared in Fig. 6. In this figure, the envelope of  $i$  as the normal current of  $i_p$  equivalent to  $i_g$  ref furthermore,  $i_{out}$  can be respected amid every exchanging cycle.

As indicated by Fig. 4, the exchanging recurrence fluctuates with in BCM operation, which is more convoluted than in DCM operation. The VSF prompts the difficulty to get the precise numerical model between  $i_{out}$  what's more,  $I$ . In the mean time, because of the prerequisites of the GT gadgets  $i_{ref}$  out should be an impeccable sinusoidal waveform, while have the same recurrence and stage with the utility. That implies the exact scientific model is extremely important.

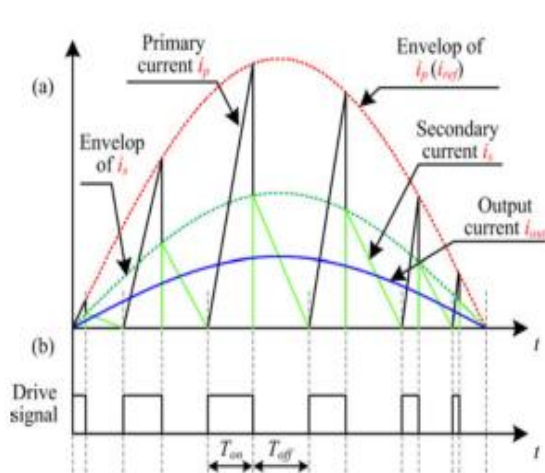


Fig 4. Relationship Between  $i_{out}$  and  $i_{ref}$  in BCM.

**F. Proposed Mathematical Model Between  $i_{out}$  and  $i_{ref}$**

The proposed scientific model in the middle of  $i_{out}$  and  $i_{ref}$  in BCM operation will be dissected through hypothetical determination with two basic presumptions as:

- 1) Since the fly back inverter works at high exchanging recurrence, UDC,  $u_g$ , and  $i_{ref}$  can be accepted as constants amid every exchanging cycle;
- 2) All the parts in the circuit are perfect, hence the spillage inductance of transformer, exchanging misfortune and other parasitic parameters of the circuit, (for example,  $C_{oss}$ ) are not considered.

As per the volt-second adjust of inductance, the turn-on and turn-off times can be communicated as (1). Furthermore, the relationship of  $I_p$  and  $I_s$  can be appeared as (2)

$$T_{on} = L_p \cdot I_p \cdot \frac{1}{U_{dc}}$$

$$T_{off} = L_s \cdot I_s \cdot \frac{1}{U_g}$$

$$I_p = I_{ref}$$

$$I_s = n \cdot I_p = I_p \sqrt{\frac{L_p}{L_s}}$$

Since  $i_{out}$  is gotten by separating the optional current  $i_s$ ,  $i_{out}$  roughly equivalents to the normal estimation of  $i_s$  amid every exchanging cycle. Along these lines, the range S1 and S2 can be thought as equivalent, as appeared in Fig. 7. Along these lines,  $i_{out}$  can be communicated as (3)

$$i_{out} = \frac{1}{2} I_s \cdot T_{off} \cdot I_s \cdot \frac{1}{T_{on} + T_{off}}$$

$$i_{out} = \frac{1}{2} \frac{I_{ref} \sqrt{\frac{L_p}{L_s}} \cdot L_s I_{ref} \sqrt{\frac{L_p}{L_s}} \cdot \frac{1}{U_g}}{I_{ref} \sqrt{\frac{L_p}{U_{dc}}} + L_s I_{ref} \sqrt{\frac{L_p}{L_s}} \cdot \frac{1}{U_g}}$$

Substituting (1) and (2) into (3), (4) can be gotten. After improvement, the perfect numerical model in the middle of  $i_{out}$  and  $i_{ref}$  can be gotten as (5).

This is the proposed scientific model, which can be connected in the single fly back inverter. As per this expression,  $i_{ref}$  is controlled by the framework voltage  $u_g$ , the data voltage UDC and the turns proportion  $n$  of transformer. In the PV ACM application, the data voltage is chosen by the PV board and information capacitor  $C_{in}$ , and there is typically a huge information capacitor that is utilized to get consistent data voltage.

In this way, UDC can be viewed as consistent in the enduring state. In this manner, the extent of  $i_{ref}$  and  $i_{out}$  fluctuates with  $u_g$  in the line-recurrence cycle as indicated by the accompanying mathematical statement:

$$I_{ref} = 2 I_{out} \left( \sqrt{\frac{L_s}{L_p}} + \frac{U_g}{U_{dc}} \right)$$

**G. Analysis of the Output Current's THD**

As indicated by the proposed scientific model, the yield current  $i_{out}$  can be controlled by the reference current  $i_{ref}$ , and  $i_{ref}$  can be gotten by substituting the statement of  $i_{out}$  into (5). Since PV ACM is a GT gadget,  $i_{out}$  ought to follow the THD prerequisite.

On the off chance that the scientific model is off base,  $i_{out}$  will be mutilated. In this manner, the exact scientific model is the way to ensure the THD of  $i_{out}$  meet the standard prerequisites.

References [17]–[19] treated the envelope of top essential current  $i_p$  as a sinusoidal waveform in BCM operation, which is like the declaration of  $i_p$  in DCM operation as appeared in (6) [34]

$$I_{ref} = 2 \sqrt{\frac{P_o}{L_p \cdot f_s}} \sin \omega t$$

Reference [17] and [19] embraced (7) as the control law of  $i_{out}$ . As indicated by these references,  $T_{on} \cdot p$  is the  $T_{on}$  interim quality alluding to the exchanging cycle that happens at the time zone of  $\omega t = \pi/2$ , and is a consistent. The statement of  $i_{ref}$  in [18] is not obviously exhibited, but rather it is like (7),



which can be demonstrated by the fifth figure of reference [18]

$$I_{ref} = 2 \frac{U_{dc}}{L_p} T_{on} \cdot \sin \omega t$$

On the off chance that these comparisons are utilized to figure the iref in BCM operation, it has little impact on the framework proficiency, however iout will be bended and THD will increment. It is confirmed by the reenactment results in Section VI-C.

**H. Further Discussions on the Proposed Mathematical Model**

As specified prior, some useful angles are not considered in the perfect scientific model. As an example, the transformer's spillage inductance is a vital component considering the framework power misfortune [12], while the QR control is a favored methodology for BCM operation to acknowledge delicate exchanging [20]. The two impact the exactness of the proposed scientific model.

The spillage inductances can be portrayed in (8). In this manner, the relationship of Ip and Is ought to be changed as (9)

$$L_p = L_{mp} + L_{ep}$$

$$L_s = L_{ms} + L_{es}$$

$$I_s = I_p \sqrt{\frac{L_{mp}}{L_{ms}}} = I_p \sqrt{\frac{L_p - L_{ep}}{L_s - L_{es}}}$$

The waveforms of the QR control, and its guideline is explained in [20]. In this figure, uds is the drain-source voltage of MOSFET SM. Contrasted with the perfect case appeared in Fig. 7, there are an extra period assigned as the QR time TQR in Fig. 9. Subsequently, Equation (3) ought to be changed into the accompanying expression:

$$I_{out} = \frac{1}{2} I_s \cdot T_{off} \cdot I_s \cdot \frac{1}{T_{on} + T_{off} + T_{QR}}$$

As per [20], TQR can be portrayed as (11). Coss is the proportionate capacitance over the MOSFET, as appeared in Fig. 5. It is clear as in (11) that TQR is dictated by the equipment parameters. Along these lines, it can be viewed as a settled dead-band time in (10). Considering the VSF control strategy in BCM operation, TQR ought to be outlined as little as could be expected under the circumstances

$$T_{QR} = \pi \sqrt{L_p \cdot C_{oss}}$$

In the wake of substituting (1) and (9) into (10), the adjusted numerical model can be gotten as (12). On the other hand, this is excessively

convoluted and hard, making it impossible to be streamlined into a direct capacity as (5), which is lethal to the acknowledgment of reference current estimation in commonsense application

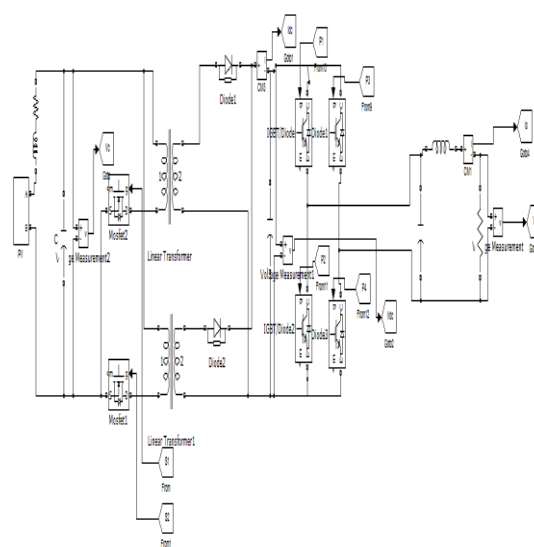
$$I_{out} = \frac{1}{2} \frac{I_{ref} \sqrt{(L_p - L_{ep}) / (L_s - L_{ms})}}{\pi (U_g / I_{ref}) \sqrt{(C_{oss} / L_s)} + (U_g / U_{dc}) \cdot \sqrt{(L_p / L_s)} + 1}$$

Additionally, the spillage inductance and the R time are not overwhelming in the framework, and they can be minimized through the equipment improvement. Along these lines, this paper utilizes the perfect scientific model, as appeared in (5), in fly back-inverter application in the wake of taking all components as a hole.

**III. PROPOSED SIMULINK SYSTEM**

The proposed model implemented with fly back converter with an inverter. The fly back converter consisted two converters individually with ideal transformers with diodes and capacitance. The presence of two fly back converters which can improve the power ratings of the system. The utilization of the transformers can reduce the voltage stress levels at secondary side and also reduces the current ripples from the fly back converter.

The fly back converter which is operated by the Hysteresis controller. The voltage which is improved effectively with the help of diodes and capacitor. The developed Simulink model which is demonstrated on the below figure.



**Fig 5: simulink model of proposed fly back converter with inverter**

The hysteresis controller which is utilized for the triggering technique for the fly back converter. Here in this strategy we took the reference voltage for the dc voltage with measure dc voltage at the output of fly back converter. There always some errors were

generated. The error signal which is modified by the presence of PI controllers.

In this process we can utilize the generated voltage from pv which is produced with the modified signal to enhance the required reference currents, this current again verified by the Idc. Finally one appropriate acute signal is delivered. The generated signal which is compared with the hysteresis controller internal threshold voltages.

Whenever the generated signal maintains increased voltages than the internal threshold voltages in that conditions hysteresis controller produces the firing pulses. These pulses pass to the fly back converter it produced voltage. This is given to the inverter. The controller diagram is given in the below figure.

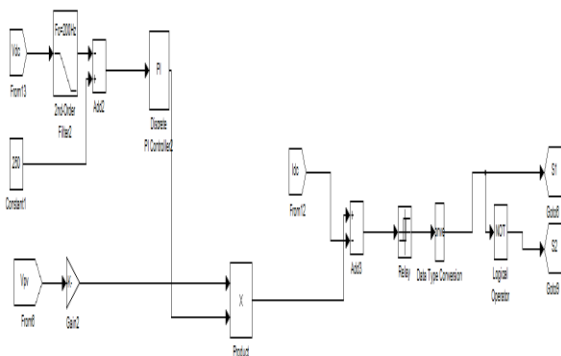


Fig 6: Hysteresis Controller For The Fly Back Converter

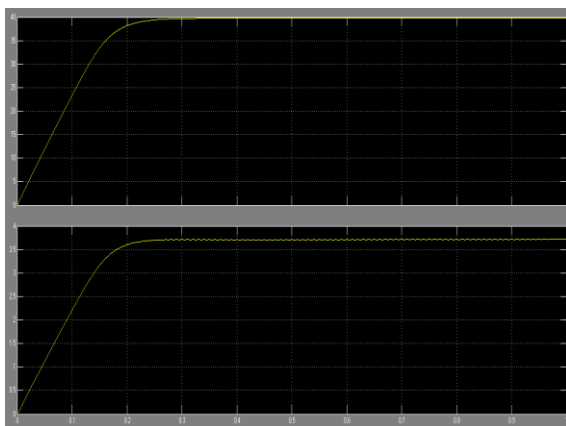


Fig 7 : The Generated Voltage and Currents from PV Array

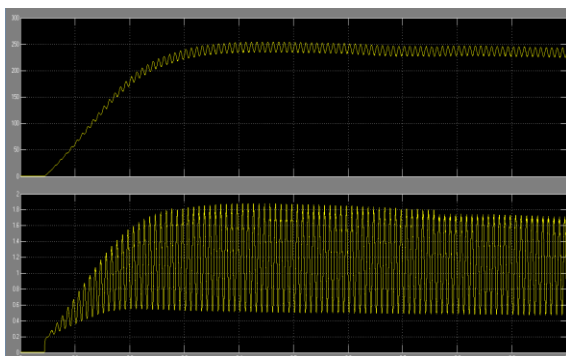


Fig 8 : The Generated Voltage and Currents from Fly Back Converter

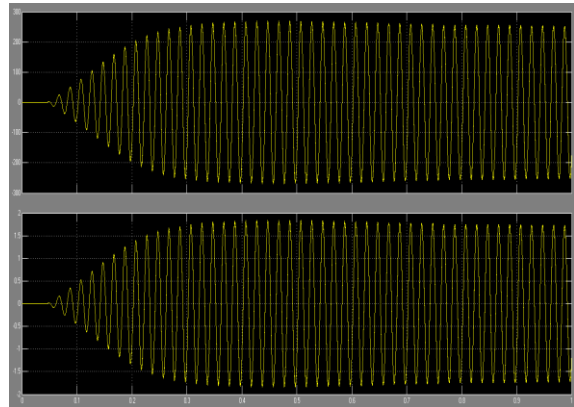


Fig 9 : The Generated Voltage And Currents From Inverter

The generated dc voltage which is fed back to the inverter. The inverter consisting of four thyristors.

Which are used to convert the dc voltages into required ac module applications. The inverter is controlled by the SPWM technique by the sine wave signal with triangular signals, finally the pulses are given to the inverter it generates ac power. Here filter parameters also utilized to reduce the ripple contents in the ac power. Finally it can maintain purified ac power from the inverter.

The generated voltage and currents at PV array are shown in fig 7. fig 8 represents the generated voltage and currents from the fly backs converter. Fig 9 gives the generated output voltages from the inverter.

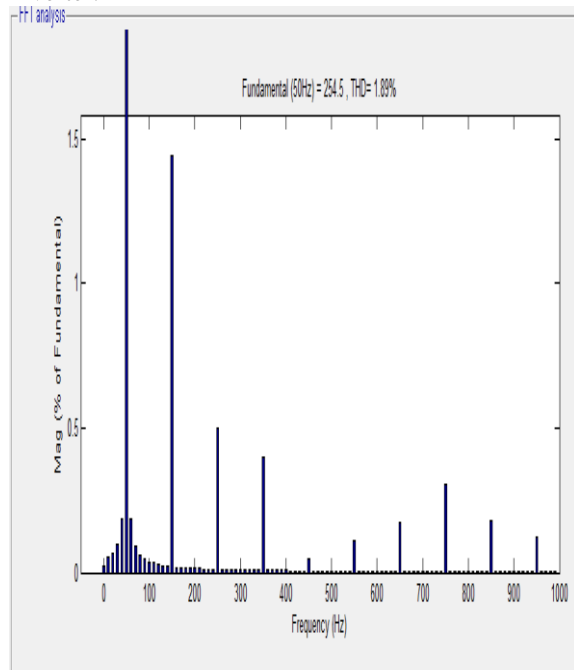


Fig 10: FFT Analysis For THD

The proposed model reduces the THD levels are shown in above figure 10. The model produced very less THD values like 1.89% which can improve the system reliability.

#### IV. CONCLUSION

Fly back inverter is a permissive clarification for photovoltaic ac application. As a grid-connected mechanism, fly back inverter must work as a current source inverter and presented the sinusoidal resultant current that is synchronous with the output voltage at grid side. In the meantime, the fly back converter must have high reliability to satisfy user's requirement.

In this technology, BCM is more suitable and preferred rather than the DCM and CCM, because of its having higher power level generations, effective performance, and efficient reliability and larger operating switching frequency bandwidth levels. But, the operating of BCM is more difficult, owing to its Variable Switching Frequency.

This also processed and produced the difficulty problems from this to get the precise mathematical simulink model between resultant output current  $i_{out}$  and required reference current  $i_{ref}$ , which has a enormous effects on THD of  $i_{out}$ .

In this suggested project, the association between ACM resultant output current  $i_{out}$  and required reference current  $i_{ref}$  of fly back converter in Barrier Control Method is implemented, and it can produce an accurate mathematical representation is suggested from the theoretical knowledge.

Subsequently, an advanced control strategy of reference current  $i_{ref}$  is implemented to reduce THD of resultant current  $i_{out}$ . Furthermore, the comprehension of Hysteresis control based on this control strategy is also investigated.

At last, the simulation and tested results of an improved fly back-inverter technology are obtainable, under the developed Hysteresis control strategy.

#### REFERENCES

- [1] W. Bower, R. West, and A. Dickerson, "Innovative PV micro-inverter topology eliminates electrolytic capacitors for longer lifetime," in Proc. Conf. Rec. 2006 IEEE 4th World Conf. Photovoltaic Energy Convers., vol. 2, May 7–12, 2006, pp. 2038–2041.
- [2] J. J. Bzura, "The AC module: An overview and update on self-contained modular PV systems," in Proc. 2010 IEEE Power Energy Soc. General Meeting, Jul. 25–29, 2010, pp. 1–3.
- [3] R. H. Wills, S. Krauthamer, A. Bulawka, and J. P. Posbic, "The AC photovoltaic module concept," in Proc. Proc. 32nd Intersociety Energy Convers. Eng. Conf. (IECEC-97), 27 Jul.–1 Aug., 1997, vol. 3, pp. 1562–1563.
- [4] E. Román, R. Alonso, P. Ibañez, S. Elorduizaparietxe, and D. Goitia, "Intelligent PV module for grid-connected PV systems," IEEE Trans. Ind. Electron., vol. 53, no. 4, pp. 1066–1073, Jun. 2006.
- [5] S. B. Kjaer, J. K. Pedersen, and F. Blaabjerg, "A review of single-phase grid-connected inverters for photovoltaic modules," IEEE Trans. Ind. Appl., vol. 41, no. 5, pp. 1292–1306, Sep./Oct. 2005.
- [6] W. Yu, C. Hutchens, J.-S. Lai, J. Zhang, G. Lisi, A. Djabbari, G. Smith, and T. Hegarty, "High efficiency converter with charge pump and coupled inductor for wide input photovoltaic AC module applications," in Proc. Energy Convers. Congr. Expo., Sep. 20–24, 2009, pp. 3895–3900.
- [7] X. Yuan and Y. Zhang, "Status and opportunities of photovoltaic inverters in grid-tied and micro-grid systems," in Proc. CES/IEEE 5th Int. Power Electron. Motion Control Conf. (IPEMC 2006), Aug. 14–16, 2006, vol. 1, pp. 1–4.
- [8] S. V. Araújo, P. Zacharias, and R. Mallwitz, "Highly efficient single-phase transformer-less inverters for grid-connected photovoltaic systems," IEEE Trans. Ind. Electron., vol. 57, no. 9, pp. 3118–3128, Sep. 2010.
- [9] N. Papanikolaou, E. Tatakis, A. Ciritis, and D. Klimis, "Simplified high frequency converters in decentralized grid-connected PV systems: A novel low-cost solution," in Proc. 9th Eur. Conf. Power Electron. Appl. (EPE'2003), Toulouse, France, Jun. 15–19, 2003, paper on CD.
- [10] A. C. Nanakos, E. C. Tatakis, and N. P. Papanikolaou, "A weighted efficiency-oriented design methodology of flyback inverter for AC photovoltaic modules," IEEE Trans. Power Electron., vol. 27, no. 7, pp. 3221–3233, Jul. 2012.
- [11] Y. Li and R. Oruganti, "A low cost fly back CCM inverter for AC module application," IEEE Trans. Power Electron., vol. 27, no. 3, pp. 1295–1303, Mar. 2012.
- [12] A. Kyritsis, N. Papanikolaou, E. Tatakis, and J. Kobougias, "Design and control of a current source flyback inverter for decentralized gridconnected photovoltaic systems," in Proc. 2005 Eur. Conf. Power Electron. Appl., Jun. 15–19, 2005, pp. 1–10.
- [13] A. Ch. Kyritsis, E. C. Tatakis, and N. P. Papanikolaou, "Optimum design of the current-source flyback inverter for decentralized grid-connected photovoltaic systems," IEEE Trans. Energy Convers., vol. 23, no. 1, pp. 281–293, Mar. 2008.
- [14] J.-Y. Gu, H.-F. Wu, G.-C. Chen, and Y. Xing, "Research on photovoltaic grid-connected inverter based on soft-switching interleaved flyback converter," in Proc. 2010 5th IEEE Conf. Ind. Electron. Appl. (ICIEA), Jun. 15–17, 2010, pp. 1209–1214.
- [15] S. J. Chiang, K. T. Chang, and C. Y. Yen, "Residential photovoltaic energy storage system," IEEE Trans. Ind. Electron., vol. 45, no. 3, pp. 385–394, Jun. 1998.