# Real Power Loss Minimization of AC/DC Hybrid Systems with Reactive Power Compensation by using Teaching Learning based Optimization Algorithm

Dr.B.Suresh Babu

Professor

Electrical & Electronics Engineering, Shri Vishnu Engineering College for Women, Vishnupur, Bhimavaram, West Godavari District, Andhra Pradesh - 534202, India.

Abstract – This Paper Presents a Teaching Learning based Optimization (TLBO) Algorithm for the Solution Real Power Loss (RPL) Minimization of AC/DC Hybrid Systems with Reactive Power Compensation . The objectives is to minimize the Real power Loss of generating units with optimal setting of control variables without violating inequality constraints and satisfying equality constraints. The DC links placed in the transmission system involve consumption of reactive power by the converters at both ends. The Reactive Power Flow can be manipulated based on the removing at the end bus it from the system. Optimal Power Flow (OPF) is an important operational and planning problem in minimizing the chosen objectives of the power system. The recent developments in power electronics allow replacing the existing transmission lines by DC links with a view of making the operation more flexible, secure and economical. The solution process involves sequential NR based AC/DC power flow. It presents simulation results of two IEEE 14 and 30 bus test systems with a view of demonstrating its effectiveness.

**Keywords**: optimal power flow, AC/DC power flow, teaching-learning based optimization, valve point effect.

h(x,u)

# **NOMENCLATURE**

NOMENCLATUR	£	$h_m$	converter transformer tap at bus- <i>m</i>
$a_i b_i c_i$	fuel cost coefficients of the $j$ -	$I_m^{dc}$	injected DC current at bus-m
b(x, u)	th generator equality constraints	$I_p^{dc}$	DC current at $p$ -th DC link
$d_j e_j$	coefficients of valve point effects of the $i$ th generator	<i>Iter</i> <sup>max</sup>	maximum number of iterations for convergence check.
50	cheets of the j-th generator	LVSI	Largest VSI
FC F	fuel cost performance, indicating the	$L_i$	VSI at load bus- i
q	fitness, of the q-th student inequality constraint	$L_p^{dc}$	location of $p$ -th DC link
$G_{mn} + jB_{mn}$	real and imaginary terms of bus	ng nt	number of generators number of transformers
	corresponding to <i>m</i> th row and	ns	number of students
	" th column	nl	number of lines
g	conductance of the transmission	nobj	number of objectives
omn	line connected between buses	OPF	optimal power flow
	<i>m</i> and <i>n</i>	OPFDC	OPF with DC link placement
<i>gD</i> ,	grade points		problem
	h	PSO	particle swarm optimization
HSU	narmony search optimization	PM	proposed method

DC link equations

$P_s^G$	real power generation at slack	$V_j^G$	voltage magnitude at $j$ -th
$P_w^{ac}$	active power transmitted from the AC system into the DC	$V_i^L$	generator bus voltage magnitude at $i$ -th load
$P_m^G$ and $Q_m^G$	system at bus- <i>w</i> real and reactive power	$V_m^{dc}$	DC link voltage at bus- <i>m</i>
$m \sim 2m$	respectively	$V_w^{ac}$	AC voltage at bus- <i>W</i>
$P_m^D$ and $Q_m^D$ $P_i^0$	real and reactive power demand at <i>m</i> -th bus respectively base case real power generation	$X_m^c$	commutating reactance of converter and/or leakage reactance of transformer at
J	at <i>j</i> -th PV bus		bus- <i>m</i>
$P_s^{\text{limit}}$	limit violated real power generation at slack generator	$\Phi(x,u)$	objective function to be minimized
$\mathbf{P}^{dc}$	DC link power at bus- <i>m</i>	$\Phi^A$	augmented objective function
$Q_i^G$	reactive power generation by $i$ -	$\delta_{mn}$	voltage angle difference between buses $m$ and $n$
$o^{c}$	th generator reactive power injection by $q$ -	$\varphi_m$	voltage angle at bus- <i>m</i> taking transformer secondary current
$\mathfrak{L}q$	th shunt compensator		as the reference
$Q_i^{ m limit}$	limit violated reactive power generation at $i$ -th generator bus	$\theta_m$	converter angle of the converter at bus- $m$
$O^{ac}$	reactive power consumed by the	λ	penalty factors
$\mathcal{Q}_{W}$	DC link transformer and	Ω	a set of load buses
	converter at bus- <i>w</i>	П	a set of generator buses
RPL	real power loss	Ψ	a set of PV buses
$\mathbf{R}^{dc}$	DC resistance of the link	3	a set of DC links
n <sub>mn</sub>	between buses $m$ and $n$	R	a set of tap changing
Sr.	loading of $i$ -th transmission	<i>V</i> (	transformers
~ Li	line	*	a set of shunt compensators
Smax	limit for loading of $i$ -th	M	
SLi	transmission line	1 <b>V1</b>	A set of lines, whose $S_{Li}$
S <sup>jk</sup> ave	mean grade of the j-th subject at k-th iteration	$\Delta S^{jk}$	violates the respective limit difference between the grade
$S^{jk}$ .	grade point of the j-th subject of		point of the teacher and the
~ teacher	the teacher at k-th iteration	•	mean grade point of the subject
TLO	teaching learning based	superscript	lower and upper limits
	optimization	"min" &	respectively
t	iteration counter	"max"	
$t_f$	teaching factor, which decides the value of mean to be		
	changed and can be either 1 or	I. IN	TRODUCTION
	2	The optimal power fl	ow (OPF) has been widely used
$T_{v}$	tap setting of $V$ -th	in power system op	eration and planning since its
UD	transformer	introduction by Carj	penter in 1962 [1]. The OPF
VP	voltage profile	control variables	entimizing a former system
VS	voltage stability	objective functions	y optimizing a new selected
V 51	voltage stability index	and inequality constr	aints for given settings of loads
V <sub>i</sub>	voltage at $l$ -th bus	and system parameter	rs. The control variables include

limit violated voltage

magnitude at i-th load bus

 $V_i^{\text{limit}}$ 

generator active powers, generator bus voltages,

transformer tap ratios and the reactive power

generation of shunt compensators. In general, the total fuel cost (FC) is commonly used as the main objective for OPF problems. However, the other objectives, such as reduction of real power loss (RPL), improvement of the voltage profile (VP) and enhancement of the voltage stability (VS) can also be included, as it has progressively become easy to formulate and solve large-scaled complex problems with the advancement in computing technologies. The equality constraints are the power flow balance equations, while the inequality constraints are the limits on the control variables and the operating limits of the power system dependent variables.

The recent developments in power electronics have introduced DC transmission links in the existing AC transmission systems with a view of achieving the benefits of reduced network loss, lower number of power conductors, increased stability, enhanced security, etc. They are often considered for transmission of bulk power via long distances. The attributes of DC transmission links include low capacitance, low average transmission cost in long distances, ability to prevent cascaded outages in AC systems, rapid adjustments for direct power flow controls, ability to improve the stability of AC systems, mitigation of transmission congestion, enhancement of transmission capacity, rapid frequency control following a loss of generation, ability to damp out regional power oscillations following major contingencies and offering major economic incentives for supplying loads. Flexible and fast DC controls provide efficient and desirable performance for a wide range of AC systems.

While most of the existing DC links are designed for point to point transmissions, the multi-terminal DC system operation has become a reality and its usage is expected to increase in future with a view of making the operation more flexible, secure and economical. The realization of multi-terminal DC systems cannot be done at once but can be executed through replacing the existing AC transmission lines by DC links over a period of time.

It is to be noted that such modernization through heuristic replacement of AC lines by DC links in the system may not be optimal and may not ensure enhanced system performance. The decision as to which of the transmission lines is to be replaced by DC links and their parameters, besides determining the optimal settings for control parameters, is of great significance in achieving the desired performances. The problem of replacing the transmission lines by DC links may be represented as "DC link placement problem". There is thus a need for extending the OPF problem to embrace the problem of placing the DC links in the existing power systems. The resulting optimization problem, designated as OPF with DC link placement problem (OPFDC), is a large scale, non-linear non-convex and multimodal optimization problem with continuous and discrete control variables. The existence of nonlinear power flow constraints and the DC link equations make the problem non-convex even in the absence of discrete control variables [2-6].

In the recent decades, numerous mathematical programming techniques such as gradient method [1], linear programming [7,8], nonlinear programming [9,10], interior point method [11-13] and quadratic programming [14] with various degrees of nearoptimality, efficiency, ability to handle difficult constraints and heuristics, have been widely applied in solving the OPF problems. Although many of these techniques have excellent convergence characteristics, they have severe limitations in handling non-linear and discontinuous objectives and constraints. The gradient method suffers from the difficulty in handling inequality constraints, and the linear programming requires the objective and constraint functions to be linearized during optimization, which may lead to the loss of accuracy. Besides they may converge to local solution instead of global ones, when the initial guess is in the neighborhood of a local solution. Thus there is always a need for simple and efficient solution methods for obtaining global optimal solution for the OPF problems.

Apart from the above methods, another class of numerical techniques called evolutionary search algorithms such as genetic algorithm [15-18], evolutionary programming [19-21], particle swarm optimization (PSO) [22-24], differential evolution [25-28], frog leaping [29], harmony search optimization (HSO) [30], gravitational search [31], clonal search [32], artificial bee colony [33] and teaching-learning [34] have been widely applied in solving the OPF problems. Having in common processes of natural evolution, these algorithms share many similarities; each maintains a population of solutions that are evolved through random alterations and selection. The differences between these procedures lie in the techniques they utilize to encode candidates, the type of alterations they use to create new solutions, and the mechanism they employ for selecting the new parents. These algorithms have yielded satisfactory results across a great variety of power system problems. The main difficulty is their sensitivity to the choice of the parameters, such as temperature in SA, the crossover and mutation probabilities in GA and the inertia weight, acceleration coefficients and velocity limits in PSO.

Recently, teaching learning based optimization (TLO) has been suggested for solving optimization problems [35,36]. It is inspired from teaching-learning process in class rooms. It mimics the behavior of the students in improving their performance through gaining the knowledge from the teacher and interacting with other students. It has been applied to a variety of power system problems [37-39] and found to yield satisfactory results.

This paper formulates the problem of OPFDC, suggests a solution methodology involving TLO with a view of obtaining the global best solution and demonstrates its performance through simulation results on IEEE 14 and 30 bus systems.

## II. TEACHING LEARNING BASED OPTIMIZATION

TLBO, inspired from teaching-learning process in class rooms, is suggested for solving multimodal optimization problems.

**Teaching Phase:** The teaching phase represents the global search property of the TLBO algorithm. In the light of the fact that the students will gain knowledge according to the quality of the teaching delivered by a teacher and the quality of the students present in the class, the mean grade point of the subject increases and the difference between the grade point of the teacher and the mean grade point of the subject is expressed as

$$\Delta S^{jk} = rand(0,1) \times \left( S_{teacher}^{jk} - t_f S^{jk ave} \right)$$
(1)

Where

 $S^{jk}$  ave is the mean grade of the j-th subject at k-th iteration and computed by

$$S^{j\,k\,ave} = \frac{1}{nS} \sum_{i=1}^{nS} S_i^{j\,k}$$
(2)

(2)  $S_{teacher}^{jk}$  is the grade point of the j-th subject of the teacher at k-th iteration

 $t_f$  is the teaching factor, which decides the value of mean to be changed and can be either 1 or 2, evaluated by

$$t_f = round([1 + rand (0,1){2-1}])$$
 (3)

The new grade point of the j-th subject of the i-th student, as a result of teaching, is mathematically modeled by

$$S_i^{j\,k+1} = S_i^{j\,k} + \Delta S^j \tag{4}$$

The grade points of all the students at the teachers phase are further improved by the learner phase.

**Learning Phase:** The learner phase stands for the local search process of the TLBO algorithm. In this phase, the students enrich their knowledge by interaction among themselves, which helps in improving their performances. In this phase, a student randomly chooses another student for interaction and enriches the knowledge through learning if the other student has more knowledge than him or her. The influence on the grade points due to the interaction of p -th student with q -th student may be mathematically expressed as follows:

$$S_{p}^{jk+1} = \begin{cases} S_{p}^{jk} + rand \times \left(S_{p}^{jk} - S_{q}^{jk}\right) & \text{if } F_{p} > F_{q} \\ S_{p}^{jk} + rand \times \left(S_{q}^{jk} - S_{p}^{jk}\right) & \text{otherwise} \end{cases}$$

(5) (5)

 $F_p$  and  $F_q$  are the performance, indicating the fitness, of the p-th and q-th student respectively. The algorithm of the TLO is narrated below.

## **III. PROBLEM FORMULATION**

The formation of the problem involves both the AC and DC sets of equations. The AC set of equations are the standard AC power balance equations whereas the DC set equations represent power, current and voltage balance equations at both DC and AC terminal buses of DC links. Moreover the DC link can be operated in different modes such as constant current, constant power, etc [4-6]. In this formulation, DC links with constant current control are considered. The OPFDC problem is formulated as a constrained nonlinear (6)

optimization problem through combining the standard OPF problem and the DC set of equations as

Minimize  $\Phi(x, u)$ 

Subject to b(x, u) = 0 (7)  $g(x, u) \le 0 (8)$ 

Where

 $x = [V_i^L, Q_j^G, P_s^G]$ , the vector of dependant variables (9)

 $u = [P_k^G, V_j^G, T_v, Q_q^C, L_p^{dc}, I_p^{dc}], \text{ the vector of}$ control or independent variables  $b(x,u) = \begin{cases} P_m^G - P_m^D - V_m \sum_{\substack{n \in \{\Omega, \Pi\}\\n \in \{\Omega, \Pi\}}}^{nb} V_n(G_{mn} \cos \delta_{mn} + B_{mn} \sin \delta_{mn}) = 0 \\ Q_m^G - Q_m^D - V_m \sum_{\substack{n \in \{\Omega, \Pi\}\\n \in \{\Omega, \Pi\}}}^{nb} V_n(G_{mn} \sin \delta_{mn} - B_{mn} \cos \delta_{mn}) = 0 \\ \\ h(x,u) = 0 \end{cases}$ 

, the equality constraints

$$g(x,u) = \begin{cases} P_k^{G(\min)} \leq P_k^G \leq P_k^{G(\max)} \\ Q_j^{G(\min)} \leq Q_j^G \leq Q_j^{G(\max)} \\ Q_q^{C(\min)} \leq Q_q^C \leq Q_q^{C(\max)} \\ T_v^{\min} \leq T_v \leq T_v^{\max} \\ V_j^{G(\min)} \leq V_j^G \leq V_j^{G(\max)} \\ V_i^{L(\min)} \leq V_i^L \leq V_i^{L(\max)} \\ I_p^{dc(\min)} \leq I_p^{dc} \leq I_p^{dc(\max)} \\ |S_{Li}| \leq S_{Li}^{\max} \end{cases} \end{cases},$$
  
the inequality constraints

(12)

$$h(x,u) = \begin{cases} V_m^{dc} - smc_2 h_m V_w^{ac} \cos\theta_m + s_m c_3 X_m^c I_m^{dc} = 0 \\ V_m^{dc} - 0.995c_2 h_m V_w^{ac} \cos\varphi_m = 0 \\ Q_w^{ac} - V_w^{ac} c_2 h_m I_m^{dc} \sin\varphi_m = 0 \\ P_w^{ac} - V_w^{ac} c_2 h_m I_m^{dc} \cos\varphi_m = 0 \\ P_m^{dc} - V_w^{ac} I_m^{dc} = 0 \\ I_m^{dc} - \left(V_m^{dc} - V_n^{dc}\right) / R_{mn}^{dc} = 0 \\ V_m^{dc} - V_n^{dc} - I_m^{dc} R_{mn}^{dc} = 0 \end{cases}$$
, the DC link equations (13)

 $S_m = 1$  for rectifier and -1 for inverter

$$\begin{split} c_2 &= 3\sqrt{2}/\pi \\ c_3 &= 3/\pi \\ i \in \Omega \text{, a set of load buses} \\ j \in \Pi \text{, a set of generator buses} \\ k \in \Psi \text{, a set of PV buses} \\ v \in \Re \text{, a set of tap changing transformers} \\ p \in \mathfrak{I}, \text{ a set of DC links} \\ q \in \aleph, \text{ a set of shunt compensators} \end{split}$$

The objective function  $\Phi(x, u)$  can take different forms.

**Minimization of Fuel Cost** 

Minimize

$$\Phi_{1}(x,u) = \sum_{j \in \Pi} a_{j} P_{j}^{G^{2}} + b_{j} P_{j}^{G} + c_{j} + \left| d_{j} \sin(e_{j}(P_{j}^{G}(\min) - P_{j}^{G})) \right|$$
(14)

Minimization of Real Power Loss Minimize

$$\Phi_{2}(x,u) = \sum_{w=1}^{nl} g_{mn} \left( \left| V_{m} \right|^{2} + \left| V_{n} \right|^{2} - 2 \left| V_{m} \right| \left| V_{n} \right| \cos \delta_{mn} \right)$$
(15)

#### **Enhancement of Voltage Stability**

The VS can be enhanced by minimizing the largest value of VS index (VSI) of load buses [40] as Minimize

$$\Phi_3(x,u) = \max\{L_i; i \in \Omega\}$$
(16)

Where 
$$L_i = \left| 1 - \sum_{j=\Pi} F_{ji} \frac{V_j}{V_i} \right|$$
 (17)

The values of  $F_{ji}$  are obtained from the bus admittance matrix.

The multi-objective OPFDC problem is tailored by combining several objectives through weight factors so as to optimize all the objectives simultaneously.

Minimize 
$$\Phi(x,u) = \sum_{i=1}^{nobj} w_i \Phi_i$$
 (18)

Where the weights w that indicate the relative significance among the chosen objectives, are small positive real values, whose sum is usually set as one.

#### **IV. PROPOSED ALGORITHM**

The proposed TLO based method involves representation of problem variables and the formation of a performance function.

### A. Representation of decision variables

The converters at both ends of the DC links draw lagging reactive power and pose a burden to the existing power system. S denotes the grade points of each student in the PM and represents the control variables in vector form as:

$$S = [P_k^G, V_j^G, T_v, I_p^{dc}];$$
  

$$j \in \Pi \quad k \in \Psi \quad v \in \Re \quad p \in \mathfrak{I}$$
(19)

#### **B.** Performance Function

The TLO searches for optimal solution by maximizing a fitness function, denoted by F, which is formulated from the objective function of Eq. (10) and the penalty terms representing the limit violation of the dependant variables such as reactive power generation at generator buses, voltage magnitude at Joad buses and real power generation at slack bus. F can be built as

$$Max \quad F = \frac{1}{1 + \Phi^A} \tag{20}$$

Where

$$\Phi^{A} = \Phi(x, u) + \lambda_{V} \sum_{i \in \Omega} \left( V_{i}^{L} - V_{i}^{\text{limit}} \right)^{2} + \lambda_{Q} \sum_{i \in \Pi} \left( Q_{i}^{G} - Q_{i}^{\text{limit}} \right)^{2} + \lambda_{P} \left( P_{s}^{G} - P_{s}^{\text{limit}} \right)^{2} + \lambda_{S} \sum_{i \in M} \left( S_{Li} - S_{Li}^{\text{max}} \right)^{2}$$

$$(2.1)$$

$$V_i^{\text{limit}} = \begin{cases} V_i^{L(\min)} & \text{if } V_i^L < V_i^{L(\min)} \\ V_i^{L(\max)} & \text{if } V_i^L > V_i^{L(\max)} \\ V_i^L & \text{else} \end{cases}$$

$$Q_{i}^{\text{limit}} = \begin{cases} Q_{i}^{G(\text{min})} & \text{if } Q_{i}^{G} < Q_{i}^{G(\text{min})} \\ Q_{i}^{G(\text{max})} & \text{if } Q_{i}^{G} > Q_{i}^{G(\text{max})} \\ Q_{i}^{G} & else \end{cases}$$

$$(23)$$

$$P_{s}^{\text{limit}} = \begin{cases} P_{s}^{G(\text{min})} & \text{if } P_{s}^{G} < P_{s}^{G(\text{min})} \\ P_{s}^{G(\text{max})} & \text{if } P_{s}^{G} > P_{s}^{G(\text{max})} \\ P_{s}^{G} & \text{else} \end{cases}$$

$$(24)$$

The power system is altered through replacing the transmission lines of  $L_p^{dc}$  with DC currents of  $I_p^{dc}$  and setting the control parameters of  $\{P_k^G, V_j^G \text{ and } T\}$  for each student. The AC/DC power flow is then run with a view of computing the objective function  $\Phi(x, u)$  and the performance function F.

### C. Repair Mechanism

It is undesirable to choose a transmission line for replacement by two or more DC links. During the iterative process, there is a possibility that a solution point may contain same line numbers in  $L_p^{dc}$  of the student for placing two or more DC links. If this happens, it may be corrected by the following repair mechanism.

Alter any one line number by generating a random number to represent another line.

Repeat the above step till no two numbers in

 $L_p^{dc}$  are the same.

#### **D.Stopping** Criterion

The process of generating new population can be terminated either after a fixed number of iterations or after some number of iterations when there has been no increase in the fitness function value.

#### E. Solution Process

An initial population of students is obtained by generating random values within their respective limits to every individual in the population. The fitness F is calculated by considering  $gp_s$  of each student; and the teaching and learning phases are performed for all the students in the population with a

view of maximizing their performances. The iterative process is continued till convergence. The pseudo code of the PM is presented below

**Read** the Power System Data **Cho Choose** the number of students in the population,

ns and Iter<sup>max</sup> for convergence check. Generate the initial population of students Set the iteration counter t = 0while (termination requirements are not met) do for i = 1: ns

• Repair the *i*-th student

- Replace the transmission lines by DC links and set the control parameters according to  $\dot{i}$ -th student values
- Run AC/DC power flow
- Evaluate the augmented objective function  $\Phi^A$  and performance function  $F_i$  using Eqs. 21 and 20 respectively

end-(i)

**Choose** the best student possessing the largest  $F_i$  in the population as the teacher

**Evaluate** the mean grade point for each subject by Eq. (2)

**Perform** the Teaching phase to modify the grade points of each student by Eq. (4)

**Perform** the Learning phase to update the grade points of each student by Eq. (5) **end**-(while)

**Choose** the best student with highest  $F_i$  in the

**Choose** the best student with highest  $\Gamma_i$  in the population as the optimal solution

### **V. SIMULATIONS**

The PM is tested on IEEE 14 and 30 bus test systems, whose data have been taken from Ref. [41]. The fuel cost coefficients, lower and upper generation limits for these two test systems are taken from Ref. [42-44] and given in Tables A.1 and A.2 of the Appendix-A. In addition, the initial generations at PV buses are altered to lie within the respective lower and upper limits as given in the Tables A-1andA-2 of Appendix-A. The sequential AC/DC power flow involving NR technique is used during the optimization process [4-6]. Programs are developed in Matlab 7.5 and executed on a 2.20 GHz Intel core-i3 personal computer. The OPFDC problem is also solved using the HSO with a view of demonstrating the efficacy of the PM.

The optimal solution obtained by the PM and HSO for test case for 14 and 30 bus systems are given through Table A.3 respectively in Appendix-A. The performances in terms of FC of PM compared with the HSO based algorithms for the test Table 3 . The table 3 also contain the base-case results, representing the performances before optimization. The transmission lines that are chosen for replacement by DC links in Table 2 for 14 and 30 bus systems . The parameters chosen for the PA are given in Table 1.

#### **Table 1 TLBO Parameter**

Parameter	Value
ns	30
<i>Iter</i> <sup>max</sup>	300

Table 2 Transmission lines replaced by DC links

System	Line No
14 bus	9
30 bus	31 and 11

**Table 3 Comparison of Performances for RPL** 

		Before Placement	PM	HSO
14	FC	834.6716	1022.2792	1022.2903
	RPL	8.9737	2.6840	2.6936
30	FC	813.6941	967.3416	967.4712
	RPL	7.0990	2.9655	3.0436

The minimization of the RPL is considered as the objective in this case. It is observed from Table 3 that the initial RPL of 8.9737 MW is reduced to 2.6840 and 2.6936 MW by the PM and HSO respectively for 14 bus system . Similarly, PM and HSO reduce the initial RPL of 7.0990 MW to 2.9655 and 3.0436 MW respectively for 30 bus system. It is very clear from the results that the offers best possible control settings with optimal dc link parameters, which minimize the RPL to the lowest possible value, when compared with those of HSO. It is to be noted that PM offers better control settings with optimal dc link parameters, resulting in lower RPL than those of HSO. The % RPL savings of PM are graphically compared with those of HSO in Figure 1 for all the test systems. It is seen from the figures that the %RPL savings of PM is greater than

those of PSO. As minimization of FC are not considered as objectives in this case, the FC are away from the respective best values for all the test systems, while reducing the RPL.





## **VI. CONCLUSION**

The study of OPF is an important analysis in power system operational planning. A multi-objective OPF with DC link placement problem is formulated and a TLO based solution strategy for the developed problem is suggested with a view to obtain the global best solution. This paper shows the Real Power Loss of AC/DC Hybrid Systems with Minimization Reactive Power Compensation. The solutions are treated as grade points of students and the best student in the population is considered as the teacher. The grade points are adjusted towards the best solution point based on the teaching and learning process. The algorithm uses sequential AC/DC load flow involving NR technique for computing the objective function during search. The Proposed Method approach is tested on IEEE 14 and 30 bus test systems. The results on the test systems project the ability of the proposed strategy to produce the global best solution involving lower computational burden. It has been chartered that the new approach for solving OPF will go a long way in serving as a useful tool in load dispatch centre.

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### APPENDIX -A

Table A.1 Generator Data for IEEE 14 bus test system

Bus	а	b	с	d	е	$P_j^{G(\min)}$	$P_j^{G(\max)}$	$Q_j^{G(\min)}$	$Q_j^{G(\max)}$
1	0.0016	2.00	150	0.063	50	50	300	-40	100
2	0.0100	2.50	25	0.098	40	20	80	-40	50
3	0.0625	1.00	0	0	0	15	50	0	40
6	0.00834	3.25	0	0	0	10	35	-6	24
8	0.025	3.00	0	0	0	10	30	-6	24

Bus	а	b	С	d	e	$P_j^{G(\min)}$	$P_j^{G(\max)}$	$Q_j^{G(\min)}$	$Q_j^{G(\max)}$
1	0.00375	2.00	0	0	0	50	200	-20	-250
2	0.01750	1.75	0	0	0	20	80	-20	100
5	0.06250	1.00	0	0	0	15	50	-15	80
8	0.00834	3.25	0	0	0	10	35	-15	60
11	0.02500	3.00	0	0	0	10	30	-10	50
13	0.02500	3.00	0	0	0	12	40	-15	60

Table A.2 Generator Data for IEEE 30 bus test system

Table A.3 Optimal Solution of P.	M for 14 bus and 30 bus system
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	IE	EE 14	IEEE 30		
	Before Placement	RPL	Before Placement	RPL	
P <sup>G</sup>	188.974 35.000 20.000 12.000 12.000	66.684032 80.000000 50.000000 35.000000 30.000000	138.539 57.560 24.560 35.000 17.930 16.910	51.365529 80.000000 50.000000 35.000000 30.000000 40.000000	
V <sup>G</sup>	1.060 1.045 1.010 1.070 1.090	1.100000 1.100000 1.082114 1.088746 1.092364	1.050 1.0338 1.0058 1.0230 1.0913 1.0883	1.100000 1.098027 1.078146 1.086575 1.087217 1.099333	
Т	0.978 0.969 0.932	1.005506 1.044602 0.982939	1.0155 0.9629 1.0129 0.9581	1.024026 0.990483 0.999349 0.972067	
$L_p^{dc}$		9		31 11	
$I_p^{dc}$		0.150796		0.100000 0.124734	

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