

Original Article

Wearable, Flag-Shape Microstrip Antenna with Slot in the Ground Plane for Medical Devices

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Abstract - This work validates a wideband antenna that can be worn for medical telematics. The flag-shaped antenna constructed of the RT-duroid material with the modified ground is 34 mm by 22 mm by 0.8 mm. In order to increase the operational bandwidth and decrease the resonant frequency of a typical rectangular patch, rectangular slots are added to the partial ground plane. Providing an impedance bandwidth (-10dB) of 200 MHz, the design works at 2.48 GHz. The suggested antenna retains high efficiency (93% at 2.49 GHz) and gain (2.50 dBi). High efficiency, moderate gain, and simple design are the primary contributions.

Keywords - Flag-shaped antenna, Medical application, Microstrip patch, Rogers RT/Duroid 5880.

1. Introduction

Due to simplicity in design, affordability, and compatibility, rectangular patch antennas are more widely used [1-5]. Antennas are frequently used in wireless devices that are small, uniform, and inexpensive [6-8]. Applications for medical monitoring employ wideband, low-profile antennas [9-12]; it has been demonstrated that bending has negligible impacts on the antenna's reflection coefficient, bandwidth, gain, and efficiency [13, 14]. A microstrip patch's layout and the benefits of semi-flexible RT/Duroid are discussed in the paper [15-17] due to the rising demand for mobile and wireless transmission [18-19]. A Planar dual-band, low-profile, dual-polarized antenna is suggested in [20], considering future 4G and 5G technologies. In [21], RT/Duroid 5880 and copper are used as the base materials in a flag-shaped microstrip patch antenna. Due to their low dielectric constant and minimal dielectric loss, RT/Duroid 5880 laminations are frequently used in high-frequency and broadband applications. RT/Duroid as the substrate material is proposed primarily for biomedical applications due to its advantages, including its use for electrical properties over a broad frequency range and suitability for high moisture environments. Utilizing a partial ground plane, the proposed design is used for both wideband [22, 23] and multiband features.

The claimed antenna area is more significant to be appropriate for wearable technology, and the previously mentioned antennas occasionally fall short in compactness,

according to the literature reviewed above, in light of compact designs. Wearable gadget antennas need to be small, light, and aesthetically pleasing. It is difficult to make a small, bendable, maximum gain linearly polarized antenna. This can be explained by the competing goals because there may not be the best solution considering all goals.

Following is the breakdown of the paper section: in subsection two, design geometry is explained; briefly, subsection 3 discusses the experimentation and fabrication results and presents comparative performance analysis; subsection 4 covers the conclusion and future scope.

2. Antenna Geometry

The top view of the suggested flag-shaped patch with an internal slit and the L-shaped ground at the antenna's bottom side is shown in Figure 1. The substrate is made of a semi-flexible substance called RT/Duroid 5880, which has a 0.8-mm diameter and ϵ_r of 2.2. A transmission line (50 ohms) supported by a portion of the ground plane excites the emitting element. The antenna's dimensions are 34 mm by 22mm by 0.8 mm. Utilizing common microstrip patch equations, the radiator's seed dimensions were determined [24-26]. The suggested antenna is an altered variant of the typical rectangle patch antenna. The antenna's total size and impedance are decreased by modifying the ground line, and the primary radiator is etched with slits. The details of the dimension of the substrate, both ground line and patch, are listed in Table 1.



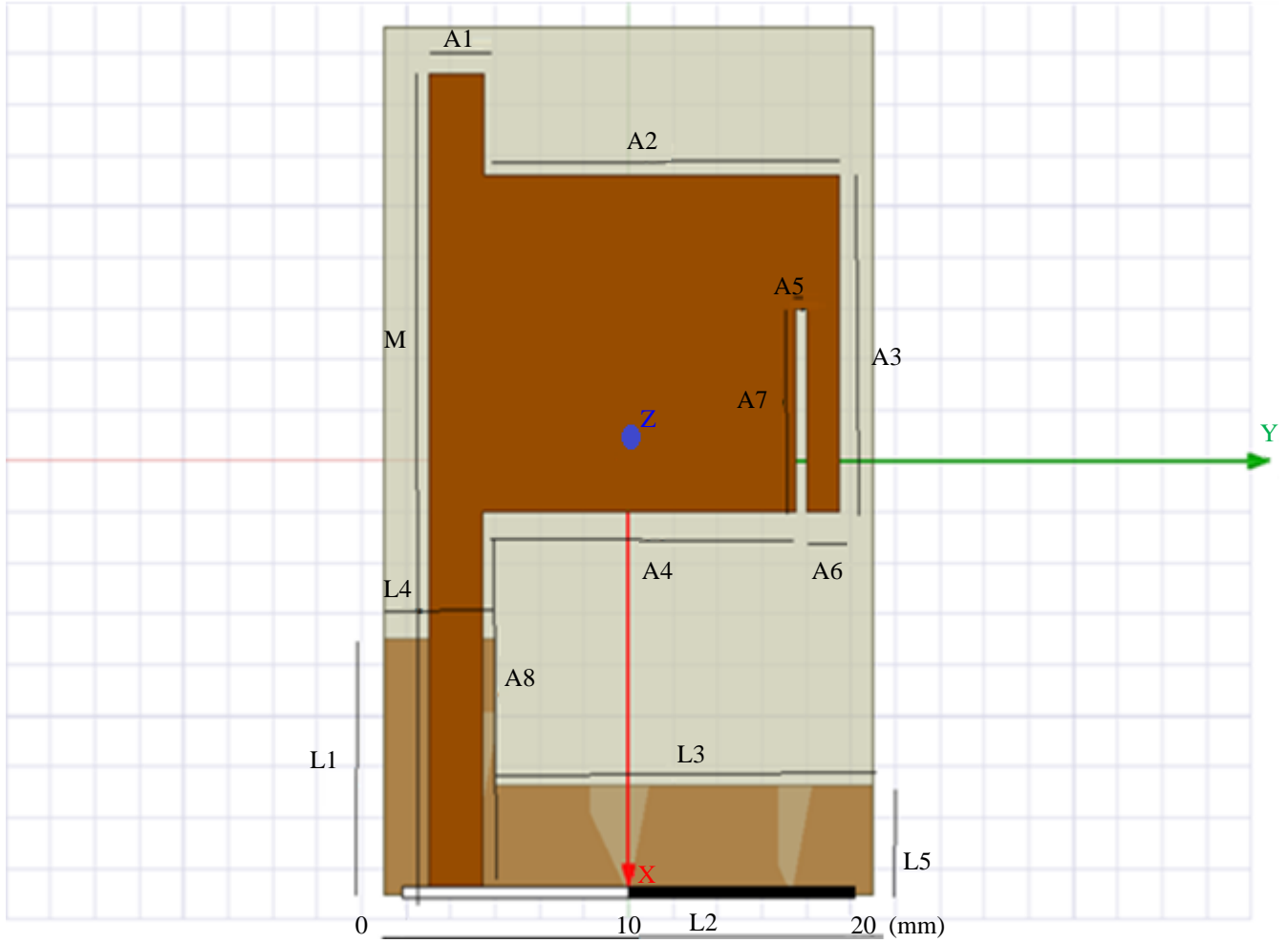


Fig. 1 Proposed flag-shaped patch on a semi-flexible antenna

Table 1. The dimension of the substrate, both ground line and patch

Specifications for Antenna	Design Elements	Size (mm)
Primary radiating patch	M	32.2
	A ₁	2.5
	A ₂	16
	A ₃	13.2
	A ₄	14.1
	A ₅	0.5
	A ₆	1.5
	A ₇	08
Ground plane	L1	10
	L2	22
	L3	17
	L4	05
	L5	4.3

3. Antenna Design and Analysis

Figure 2 shows the design evolution stages. A straightforward rectangle patch antenna with a truncated ground plane served as the basis for the design taking the reference of a monopole flag-shaped patch with partial. Ground plane [21]. The antenna had a resonance in that iteration I at about 2.8 GHz, however, the antenna's fit with the resonance frequency was poor. In iteration II, a rectangular section was connected to the top of the patch to accomplish matching impedance and miniaturization. In iteration II, the antenna had a resonance at 2.6 GHz. In iteration III, the antenna was further altered by removing a rectangular section of the long slit from the patch's bottom side and the 2.5 GHz. resonance frequency in iteration III was achieved. In iteration IV, the antenna underwent a few modifications. An additional stub resonator in the form of a rectangle was coupled to the ground plane to lengthen it. By including in the ground plane, a rectangle resonator, the antenna's 10 dB bandwidth was also boosted. The antenna used in iteration IV (the suggested antenna) operated at 2.48 GHz with an impedance bandwidth (-10dB) of 200 MHz.

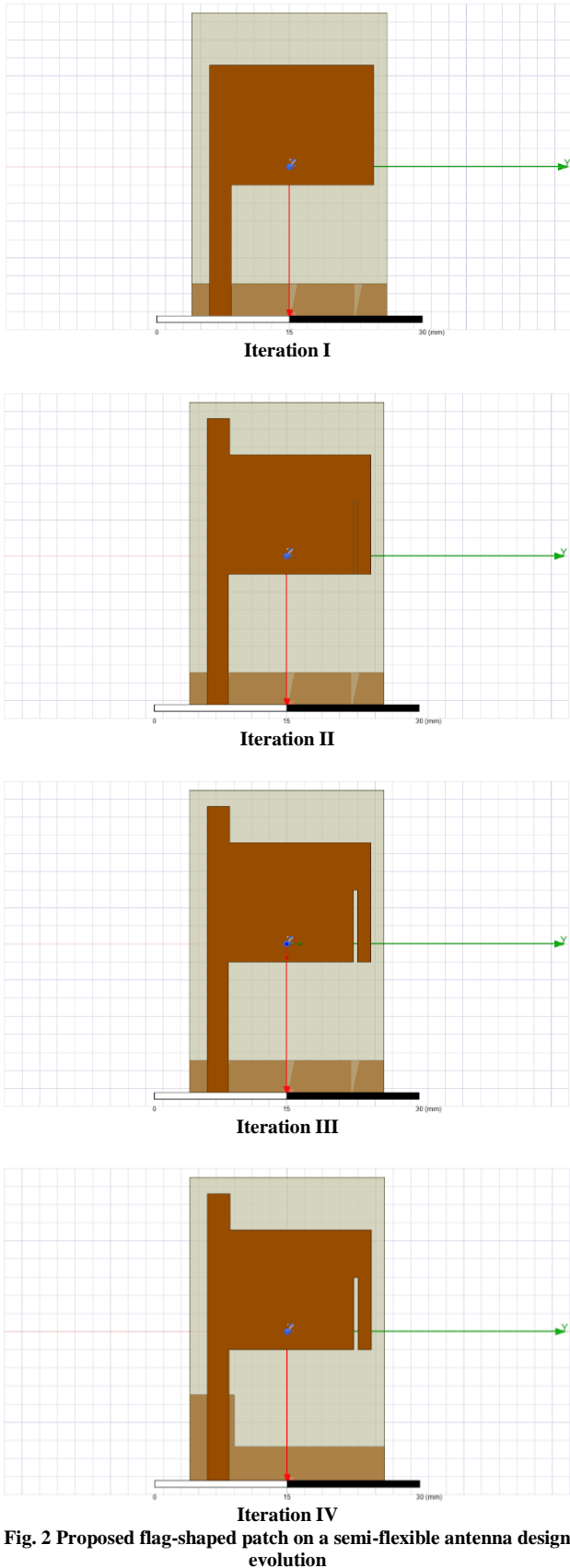


Fig. 2 Proposed flag-shaped patch on a semi-flexible antenna design evolution

The dimensions and position of the ground line and the emitting element determine how well a monopole antenna resonates. Full-wave electromagnetic simulator (HFSS 20) was used to optimize the evolution stages of the radiator and ground plane of the antenna for improved 2.48 GHz impedance matching and broad impedance bandwidth.

A simulation was conducted using HFSS 20 software after design iterations for a patch in the form of a flag. The suggested flag-shaped semi-flexible patch's return loss plot for the simulated trial versus frequency is shown in Figure 3. The generated 2D and 3D gain plots and Smith chart of a flag-shaped semi-flexible patch are shown in Figures 4, 5 and 6, respectively. It is clear from testing that the chosen design yields the best results considering the return loss parameter vs frequency response. After simulating the trial, it was discovered that the return loss was -11.68 dB at 2.49 GHz, with a 2.5 dB gain and 200 MHz bandwidth.

4. Fabrication Results and Analysis of Comparative Performance and Experimentation

The proposed antenna was developed using RT/Duroid 5880 (dielectric constant = 2.2) semi-flexible material, as shown in Figure 7 (front and rear sides). The suggested antenna was characterized using the Vector Network Analyzer (VNA) from Keysight Technologies (50 SMA connection to the microstrip line input). A measurement was made of the antenna's free-space reflection coefficient. Figure 8 shows the reflection coefficient in space and the resonant frequency. At the operating band, the findings from simulation and measurement agreed with the bandwidth of 200 MHz and 500 MHz, respectively. Figure 9 shows the Smith chart plot of the fabricated prototype where the impedance of 50 ohms is matched as per the antenna requirements. Table 2 contrasts the work's simulated and measured outcomes for better understanding—the measured findings and the simulation's result line up perfectly. A comparison of the work's simulated and measured results is displayed in Table 2 for better comprehension—the measured findings and the simulation's result line up perfectly. Table 3 contrasts the suggested design's compactness and simplicity with the other researchers' reported work.

Table 2. Simulations and measurements outcomes comparing table

Parameters of comparison	Resonant frequency	Bandwidth	Reflection-coefficient
Simulated Results	2.48 GHz	200 MHz	-11.68 dB
Measured Results	2.477 GHz	500 MHz (approx.)	-32.21 dB

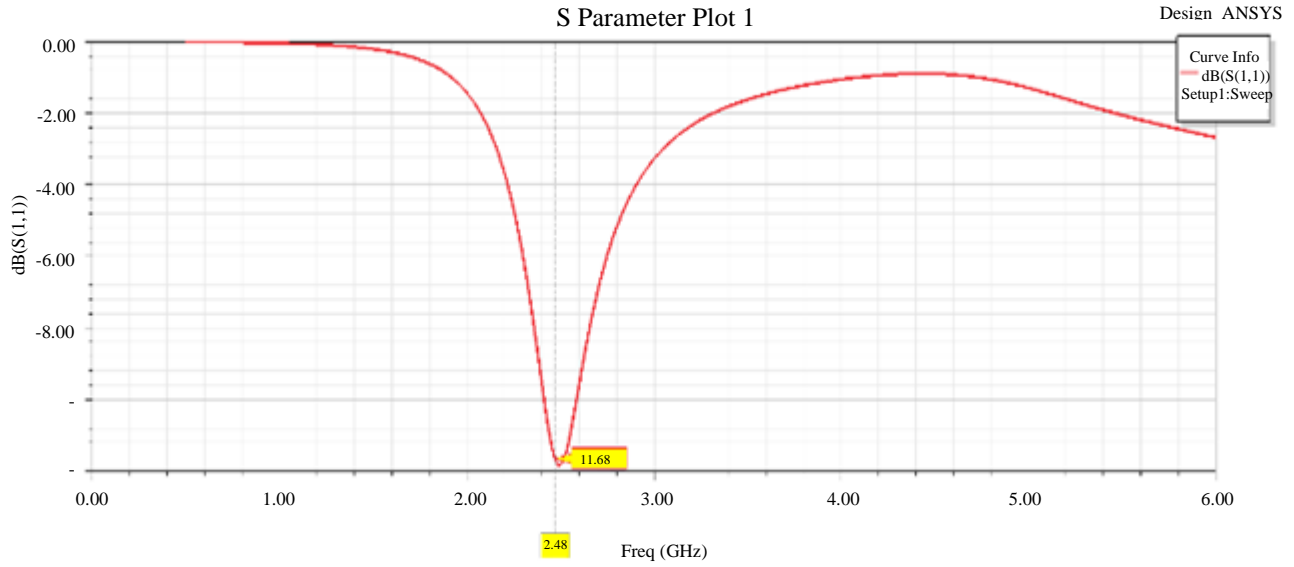


Fig. 3 Results from a simulation for a flag-shaped patch's reflection coefficient versus frequency

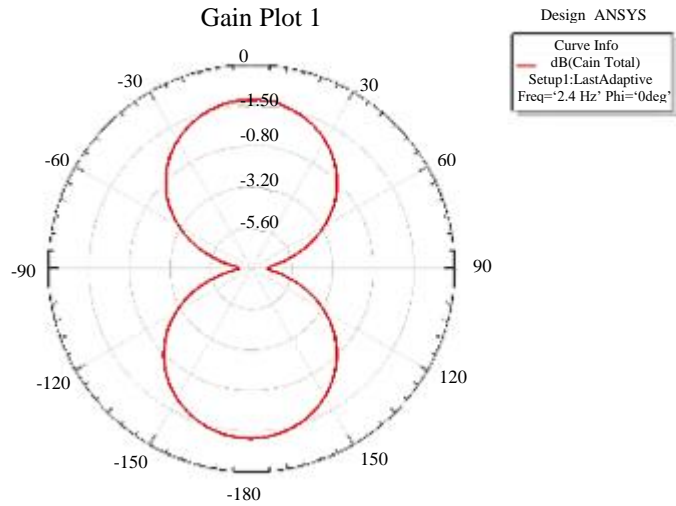


Fig. 4 Results of a 2D gain plot simulation of the flag-shaped patch

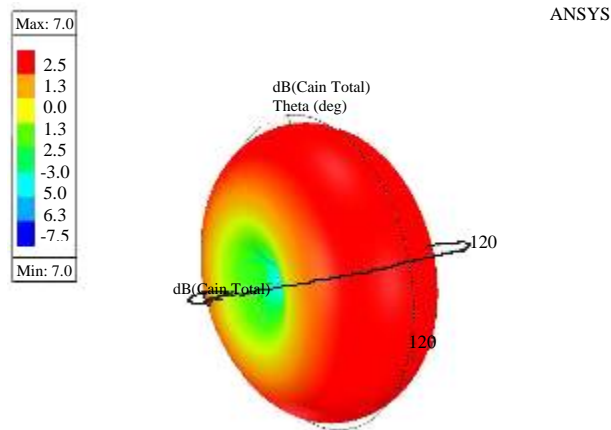


Fig. 5 Results of a 3D gain plot simulation of the flag-shaped patch

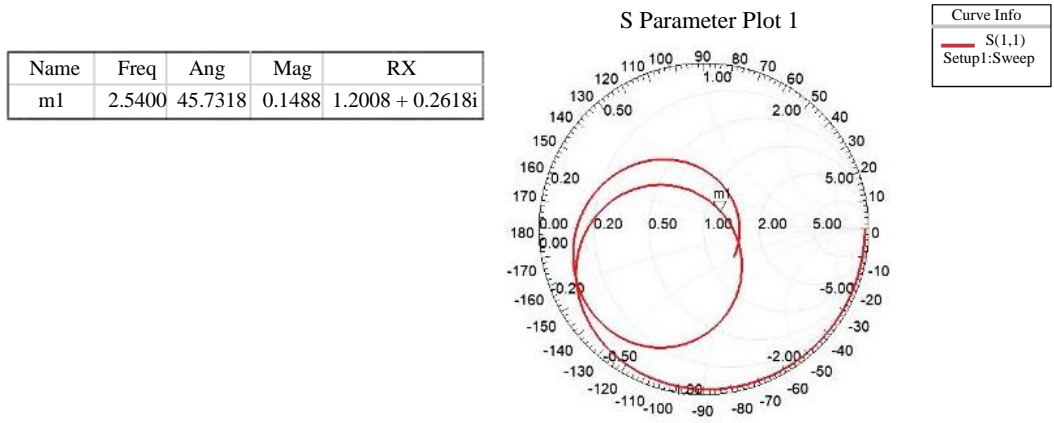


Fig. 6 Smith chart plot of the proposed design

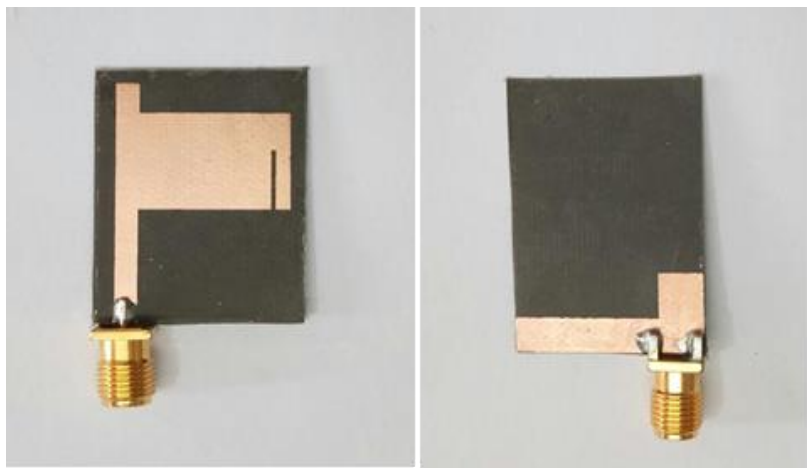


Fig. 7 Front and back view of a fabricated prototype of a flag-shaped patch

Table 3. Comparing the suggested prototype with existing literature

Parameter	[27, 28]	[29]	[30]	Suggested prototype
Antenna Dimensions (mm)	150 x 150 x 1.6	39 x 39 x 0.503	60.63× 60.63 × 0.16	34 x 22 x 0.8
Resonant Frequency (GHz)	2.45	2.45	0.762	2.47
Substrate Material	Rogers RT5880	Rogers RT5880	Rogers RT5880	Rogers RT5880
Gain	10.17 dBi	2.06dBi	1.2 dBi	2.5 dBi
Bandwidth	120 MHz	7.75% impedance bandwidth	0.759 to 0.767 GHz	500 MHz
Antenna Design	Rectangular ring patch	Koch fractal geometry	Split-ring resonator (SRR)	Flag Shaped Patch
Design Complexity	Complex	Complex	Complex	Simple

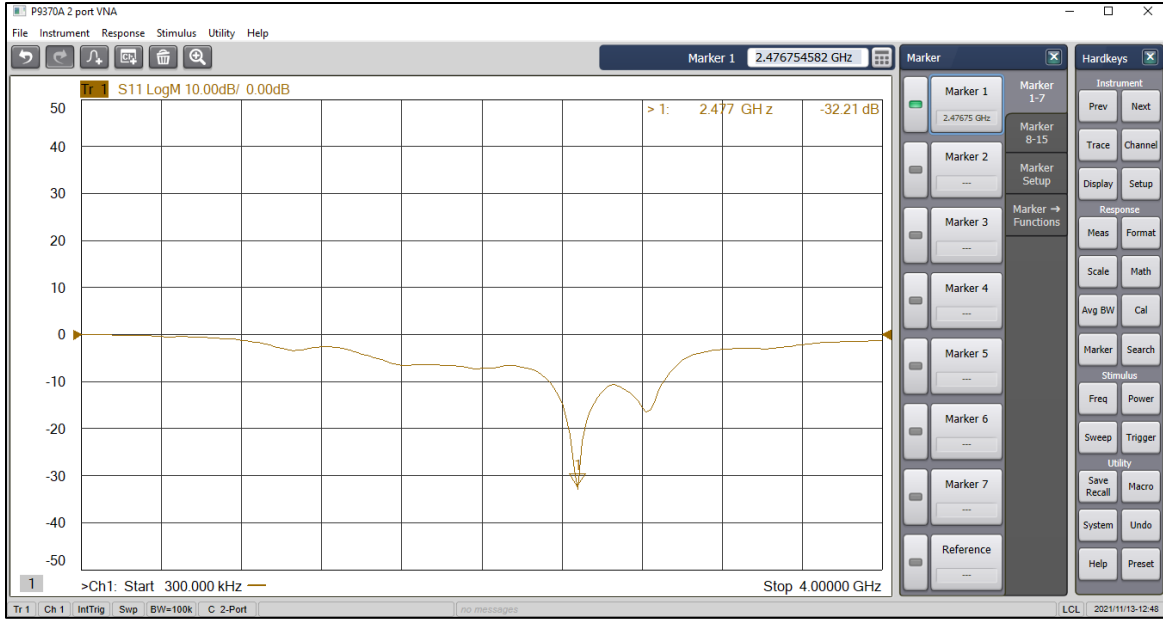


Fig. 8 Return loss plot of flag-shaped patch prototype

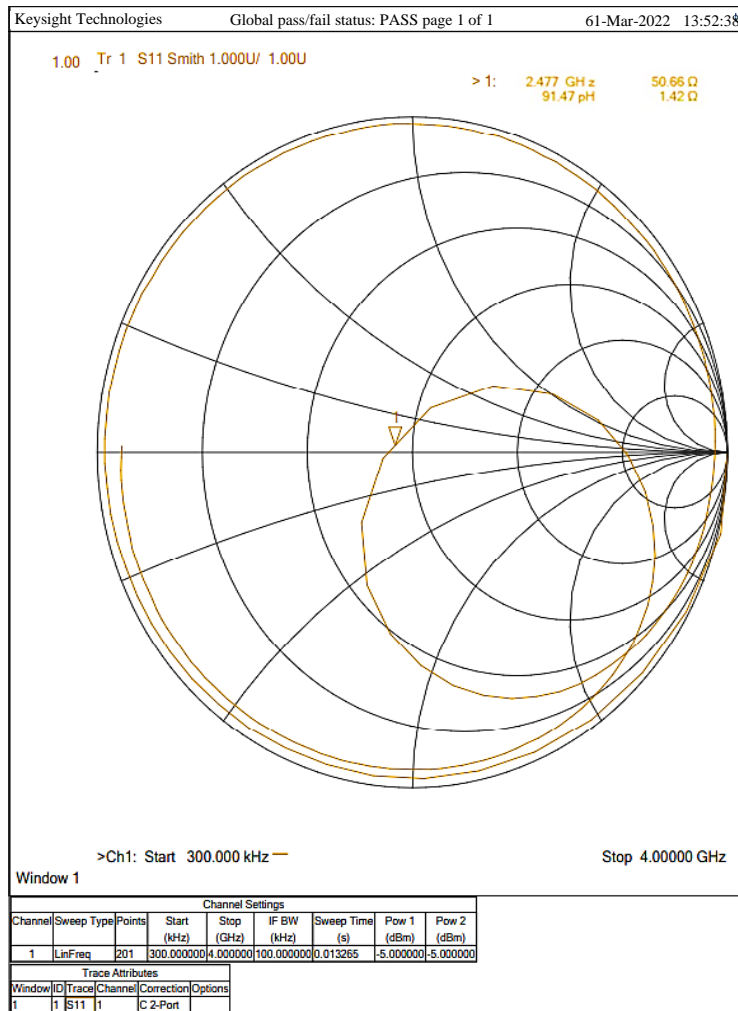


Fig. 9 Smith chart plot of flag-shaped patch prototype

5. Conclusion

For wearable biomedical equipment, a low-profile, wideband antenna is demonstrated. Adding rectangular slits to the traditional rectangle patch made it possible to miniaturize the antenna and boost the bandwidth by coupling a rectangular-shaped resonator to the ground line. With a bandwidth of 200 MHz, the designed antenna reverberated at 2.48 GHz. The suggested antenna maintained an acceptable gain and impedance matching in the open air. Due to its small size, semi-flexibility, and gain, the suggested wideband antenna is a favourite selection for wearable technology.

Between simulated and measured findings, there was a good agreement. Regarding planar solid-state devices, this design is lightweight, simple to manufacture, and suitable for mass manufacturing. The suggested method's use in the design of adaptable antennas would be the subject of further study.

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